

# Kinetic Theory of Aggregation in Granular Flow

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*This article presents a mathematical formulation of the aggregation kinetics in granular flow. The traditional kinetic theory and its generalized application to granular flow does not allow for particle size to change with time thus cannot be used to describe particle flow with aggregation taking place. In this article, a collision success factor, quantifying the completely inelastic collision of particles, is introduced into the evaluation of collision rate. The kinetic transport equations are then transformed to include source terms that account for the effects of particle size and aggregation. The analytical solution of the collision success factor is obtained by integrating the relative velocity distribution function over its velocity domain from 0 to a critical value, which corresponds a balance between the repulsion and attraction forces in a collision. The factor has been found to depend on the mixture granular energy and the critical relative collision energy. © 2011 American Institute of Chemical Engineers AICHE J, 57: 3331–3343, 2011*

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## Introduction

Attributed to the original work of Maxwell<sup>1,2</sup> and Boltzmann,<sup>3</sup> and further interpreted by Chapman<sup>4,5</sup> and Enskog,<sup>6</sup> kinetic theory was developed to describe the transport properties and constitutive relations of gases.<sup>7</sup> This theory was later generalized and applied to the flow of granular materials, which consist of particulates in granular scale flowing in a system under conditions such as fluidization or shear, to study the behavior and properties of granular particles.<sup>8</sup> As the work of Bagnold<sup>9</sup> studying the collisions of identical spherical particles on the effects of mean shear rate on momentum and collision frequency, the application of kinetic theory of granular flow has been extensively investigated in engineering<sup>10–14</sup> and fundamental physics.<sup>15–22</sup> Blinowski<sup>23</sup> and Ogawa<sup>10</sup> formulated a theoretical work using velocity fluctuation. Jenkins and Savage<sup>16</sup> attempted to extend the theory to less elastic but identical and spherical particles. They obtained the balance equations by using a pair distribution function. Further attempts<sup>24,25</sup> were also made to

describe a dense binary and nearly elastic mixture of the granular flow of spherical particles and to compare the kinetic theory predictions with the discrete element simulation using the constitutive relations for dense granular flow.<sup>26</sup> A review on the application of kinetic theory to gas fluidized beds with monodispersed particles can be found in the work of Gidaspow.<sup>27</sup> As pointed out by Sundaresan,<sup>28</sup> formidable challenges still remain in developing continuum models to include particle size distribution to address the balances of the transport properties to predict the structure such as clusters and streamers of granular particles in various flow systems.<sup>28,29</sup>

Despite the broad studies of kinetic theory and its constitutive relations on granular flows,<sup>22,26,30–42</sup> it is still true to say that the granular particles in such flows do not occur aggregation, that is, completely inelastic collision; however, in granular flows with particle aggregation such as in fluidized bed granulation,<sup>43,44</sup> it is strongly necessary to take the completely inelastic collision into account in the configuration of kinetic transport equations so as to allow the kinetic theory able to predict the change of kinetic transport properties of particles such as the number density of particles in terms of their sizes in multiple dispersed granular flow systems.

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The work presented in this article is aimed to fundamentally reconstruct the transport equations in kinetic theory to allow particle aggregation to take place so that the theory can be applied to the particle size enlargement processes induced by aggregation. This gives rise to the evaluation of the collision rate that will have to take into account the completely inelastic collisions so that the kinetic transport equations can include the source terms that are to do with aggregation.

## Assumptions

To carry out the evaluation of the collision rate and to form the kinetic transport equations, several assumptions are made as follows.

### 1. Inelastic and completely inelastic collisions.

It is allowed while some collisions between particles deviate slightly from full elasticity—characterized by a coefficient of restitution—other collisions result in a completely inelastic process after which the colliding particles adhere to each other and can be said to have aggregated and led to size enlargement, characterized by a collision success factor  $\psi$ .

### 2. Binary collision mechanism.

To evaluate the collision rate, the mechanism of the binary collision<sup>1</sup> is adopted, because it is valid in relatively dilute systems.<sup>45</sup> This suggests when the concentration of granular particles becomes dense and the mode that the motion of particles is induced can be identified, for instance by shear or by fluidization, it is necessary to replace the binary collision mechanism with the related ones such as the shear induced coagulation,<sup>46</sup> the ortho-kinetic aggregation,<sup>47</sup> Brownian motion,<sup>46</sup> and some others as can be found in the work of Williams and Loyalka<sup>48</sup> in order for the constitutive relations and relevant transport equations of the theory to be valid in and applied to the specific particulate systems.

### 3. Maxwell's distribution of particles' velocity.

The distribution of particles' velocity used in this article to derive the kinetic transport equations is regarded as Maxwellian. This distribution function captures the main features of the distribution of particles in velocity although it is the equilibrium form in Boltzmann's H-theorem.<sup>49</sup> It is thought that it is reasonable to start with this function to see the effects of the completely inelastic collisions on the velocity properties of the particles.

4. There is a critical relative collision velocity for the attraction and repulsion forces to reach a balance. Any collision with relative velocity smaller than that will lead to aggregation.

In particulate systems, where conditions exist to allow aggregation to occur that is for some of the collisions to be completely inelastic, it is understood that some mechanism must generate sufficient attraction force to overcome the repulsion force that would otherwise make the particles rebound. Because the exchange of the momentum takes place during a collision and the forces are essentially the rates of the exchanged momentum, it follows that the two forces must relate directly to and can be parameterized in terms of the initial relative velocity of two colliding particles. Here, we assume that there is a critical relative collision velocity at which point the balance between the

attraction and the repulsion forces is reached. This critical velocity indicates the maximum possibility from 0 to which two colliding particles could adhere to become an aggregate. This means that all the collisions between two kinds of particles having an initial relative velocity smaller than the critical one will lead to aggregation.

## Velocity-Size Distribution Function and Its Transport Properties

$f(v, \mathbf{c}_v, \mathbf{r}, t)$  is defined as the probability density function of particles with  $v$  ( $v$  is regarded as the volume of individual particles, hereafter throughout the article "particles  $v$ " means "particles of volume  $v$ "),  $\mathbf{c}_v$  (the velocity of particles  $v$ ),  $\mathbf{r}$  (spatial coordinates), and  $t$  (time) as the variables and is denoted as  $f_v$ . It is also called the velocity-size distribution function in this article as velocity and size are its two main characteristics and all the derivations made in this article are concerned with the properties of the two characteristics. Then, the number density of particles  $v$ ,  $n_v$ , is

$$n_v = n(v, \mathbf{r}, t) = \int_{c_v} f_v d\mathbf{c}_v. \quad (1)$$

The total number of particles per unit spatial volume located in position  $\mathbf{r}$  at time  $t$ ,  $N$ , is

$$N(\mathbf{r}, t) = \int_v n_v dv, \quad (2a)$$

and the total volume fraction  $\varepsilon_s(\mathbf{r}, t)$  and mass density  $\varepsilon_s \rho_s$  ( $\rho_s$  is the average density of all particles) of the particles are

$$\varepsilon_s = \int_v v n_v dv, \quad (2b)$$

$$\varepsilon_s \rho_s = \int_v m_v n_v dv = \int_v \rho_v v n_v dv. \quad (2c)$$

where  $\rho_v$  is the density of particles  $v$ . Let  $\phi_v = \phi(v, \mathbf{c}_v, \mathbf{r}, t)$  be a property of particles  $v$  in terms of their velocity, its ensemble average value,  $\langle \phi_v \rangle = \langle \phi \rangle(v, \mathbf{r}, t)$ , along the velocity coordinate, is

$$\langle \phi_v \rangle = \frac{\int_{c_v} \phi_v f_v d\mathbf{c}_v}{\int_{c_v} f_v d\mathbf{c}_v} = \frac{\int_{c_v} \phi_v f_v d\mathbf{c}_v}{n_v}. \quad (3)$$

The ensemble average velocity of the particles  $v$ ,  $\mathbf{u}_v = \mathbf{u}(v, \mathbf{r}, t)$ , thus becomes

$$\mathbf{u}_v = \langle \mathbf{c}_v \rangle = \frac{\int_{c_v} \mathbf{c}_v f_v d\mathbf{c}_v}{n_v}. \quad (4)$$

$\mathbf{u}_s = \mathbf{u}(\mathbf{r}, t)$  is the bulk velocity of all particles in position  $\mathbf{r}$  at time  $t$  calculated as

$$\mathbf{u}_s = \frac{\int_v \mathbf{u}_v v n_v dv}{\int_v v n_v dv} = \frac{\int_v \mathbf{u}_v v n_v dv}{\varepsilon_s}. \quad (5)$$

According to (5), the fluctuation velocity  $\mathbf{C}_v$  is defined

$$\mathbf{C}_v = \mathbf{c}_v - \mathbf{u}_s. \quad (6)$$

The granular energy of particles  $v$ ,  $\theta_v = \theta(v, \mathbf{r}, t)$ , and the mixture granular energy of all particles,  $\theta_s = \theta(\mathbf{r}, t)$ , are defined as

$$\theta_v = \frac{1}{3} m_v \langle C_v^2 \rangle, \quad (7)$$

$$\theta_s = \frac{\int_v \theta_v n_v dv}{\int_v n_v dv} = \frac{\int_v \theta_v n_v dv}{N}. \quad (8)$$

The diffusion velocity of particles  $v$ ,  $\mathbf{w}_v = \mathbf{w}(v, \mathbf{r}, t)$ , can be expressed

$$\mathbf{w}_v = \langle \mathbf{C}_v \rangle = \mathbf{u}_v - \mathbf{u}_s, \quad (9a)$$

and the mixture diffusion velocity of all particles according to (5) is

$$\frac{\int_v \mathbf{w}_v v n_v dv}{\int_v v n_v dv} = \frac{\int_v (\mathbf{u}_v - \mathbf{u}_s) v n_v dv}{\varepsilon_s} = \mathbf{u}_s - \mathbf{u}_s = 0. \quad (9b)$$

A number density weighted diffusion velocity,  $\mathbf{w}_s = \mathbf{w}(\mathbf{r}, t)$ , is also defined as

$$\mathbf{w}_s = \frac{\int_v \mathbf{w}_v n_v dv}{\int_v n_v dv} = \frac{\int_v \mathbf{w}_v n_v dv}{N}. \quad (9c)$$

We now consider  $f_v$  for in a granular flow system, the Boltzmann's equation is written as

$$\frac{\partial f_v}{\partial t} + \frac{\partial}{\partial \mathbf{r}} \cdot \mathbf{c}_v f_v + \frac{\partial}{\partial \mathbf{c}_v} \cdot \frac{\mathbf{F}_v}{m_v} f_v + \frac{\partial}{\partial v \mathbf{k}} \cdot \mathbf{G}_v f_v = r_v. \quad (10)$$

where  $\mathbf{F}_v$  is the external force imposed on particles  $v$  to maintain the flow of these particles and is a function of  $\mathbf{c}_v$ ;  $\mathbf{G}_v$  is called the growth rate and is a function of  $v$ .  $\mathbf{G}_v = dv \mathbf{k} / dt$ , here  $\mathbf{k}$  denotes the unit vector, its direction is corresponding to that defined by the spatial coordinates,  $\mathbf{r}$ , for instance Cartesian, cylindrical, or spherical system. It should be noted at this point, for the case that only aggregation is occurring,  $\mathbf{G}_v = 0$  (means no molecular deposition on particles taking place). However, we still take  $\mathbf{G}_v$  into further consideration without losing its general applicability.

For the property  $\phi_v$  of particles  $v$ , the rate of the change of this property can be obtained by integrating (10) over the velocity domain. According to (3), the Maxwell's transport equation is given by

$$\begin{aligned} \frac{\partial \langle n_v \phi_v \rangle}{\partial t} + \frac{\partial}{\partial \mathbf{r}} \cdot n_v \langle \phi_v \mathbf{c}_v \rangle - n_v \left\langle \frac{\partial \phi_v}{\partial t} \right\rangle - n_v \left\langle \frac{\partial \phi}{\partial \mathbf{r}} \cdot \mathbf{c}_v \right\rangle \\ - n_v \left\langle \frac{\partial \phi_v}{\partial \mathbf{c}_v} \cdot \frac{\mathbf{F}_v}{m_v} \right\rangle + \frac{\partial}{\partial v \mathbf{k}} \cdot n_v \langle \phi_v \mathbf{G}_v \rangle - \left\langle \frac{\partial \phi_v}{\partial v \mathbf{k}} \right\rangle \cdot n_v \mathbf{G}_v \\ = \int_{c_v} \phi_v r_v d\mathbf{c}_v. \end{aligned} \quad (11a)$$

Rearranging (11a), we have

$$\begin{aligned} \frac{\partial \langle n_v \phi_v \rangle}{\partial t} + \frac{\partial}{\partial \mathbf{r}} \cdot n_v \langle \phi_v \mathbf{c}_v \rangle + \frac{\partial}{\partial v \mathbf{k}} \cdot n_v \langle \phi_v \mathbf{G}_v \rangle \\ = \int_{c_v} \phi_v r_v d\mathbf{c}_v + n_v \left\langle \frac{\partial \phi_v}{\partial t} \right\rangle + n_v \left\langle \frac{\partial \phi}{\partial \mathbf{r}} \cdot \mathbf{c}_v \right\rangle \\ + n_v \left\langle \frac{\partial \phi_v}{\partial \mathbf{c}_v} \cdot \frac{\mathbf{F}_v}{m_v} \right\rangle + \left\langle \frac{\partial \phi_v}{\partial v \mathbf{k}} \right\rangle \cdot n_v \mathbf{G}_v. \end{aligned} \quad (11b)$$

On the left hand side of (11b), the first two terms describe the overall change of  $\phi_v$ , which is associated with the number density  $n_v$  of particles  $v$ , in time and spatial coordinates; the third term explains the change of  $n_v$  associated with  $\phi_v$  in particle size coordinate owing to the change of the particle size itself.

The terms on the right hand side of (11b) account for the sources for the rate of the changes given on the left hand side of this equation. Thus, on the right hand side of (11b), the first term describes the change of  $\phi_v$  attributed to the collisions that result in the change of number density of particles  $v$  with respect to their velocity and size characteristics; the second and third terms explain the change of  $\phi_v$  itself in time and spatial coordinates; similarly the fourth and fifth terms describe the change of  $\phi_v$  itself in velocity and size coordinates due to the external force  $\mathbf{F}_v$  and the growth of particle size. It should be noted that on the left hand side of (11b), the overall rate of change of  $\phi_v$  due to  $\mathbf{F}_v$  in velocity coordinate,  $\int_{c_v} \frac{\partial}{\partial \mathbf{c}_v} \cdot \phi_v \frac{\mathbf{F}_v}{m_v} f_v d\mathbf{c}_v$ , did not appear; this is due to the convergence of  $\phi_v \frac{\mathbf{F}_v}{m_v} f$  as  $\mathbf{c}_v$  approaches  $\infty$  and  $-\infty$ .

It is worth mentioning that  $r_v d\mathbf{c}_v$  describes the rate of change of particles  $v$  in the velocity ranging from  $\mathbf{c}_v$  to  $\mathbf{c}_v + d\mathbf{c}_v$ , as a result,  $\phi_v r_v d\mathbf{c}_v$  represents the rate of change of the property  $\phi_v$  due to the change of the number of particles  $v$  resulting from collisions. Thus,  $\int_{c_v} \phi_v r_v d\mathbf{c}_v$  measures the rate of change of  $\phi_v$  carried by all the particles  $v$  through their velocity space. We then have

$$\int_{c_v} \phi_v r_v d\mathbf{c}_v = \Delta \langle n_v \phi_v \rangle = n_v \Delta \langle \phi_v \rangle + \langle \phi_v \rangle \Delta n_v. \quad (12)$$

It is seen from (11a) with (12), by replacing  $\phi_v$  with 1,  $m_v$ ,  $m_v \mathbf{c}_v$ , and  $m_v \mathbf{c}_v^2 / 2$ , the number and mass continuity, the momentum, and the kinetic energy equations can be generated, respectively. Notwithstanding this, for systems with the change of number density of particles  $n_v$  taking place due to such as aggregation, or the ensemble average property  $\langle \phi_v \rangle$  not conserved, for example, the kinetic energy in inelastic collisions, the right hand side of this equation must be evaluated thus requires  $f_v$  to be known.

## Collision Rate and the Transport of a Property of Particles

For the particles specified by size  $v$  and velocity  $\mathbf{c}_v$ , the rate of collisions is considered in such a way that contributes in quantity to these two characteristics. The detailed derivation of the collision rate and the transport of a property of particles is given in Appendix. Here, we only describe those results. The collision rate is written as

$$\begin{aligned} r_v = \int \int \int [e_{ev}^2 (1 - \psi'_{ev}) f'_v f'_e g'_{ev} - (1 - \psi_{ev}) f_v f_e g_{ev}] \\ \times \frac{\sigma_{ev}^2}{4} (\mathbf{c}_{ev} \cdot \mathbf{k}) d\Omega d\mathbf{c}_e d\varepsilon + \int_0^v \int \int \frac{1}{2M_{v-e}^2} \psi_{e,v-e} f_{v-e} f_e g_{e,v-e} \\ \times \frac{\sigma_{e,v-e}^2}{4} (\mathbf{c}_{ev} \cdot \mathbf{k}) d\Omega d\mathbf{c}_e d\varepsilon - \int \int \int \psi_{ev} f_v f_e g_{ev} \frac{\sigma_{ev}^2}{4} (\mathbf{c}_{ev} \cdot \mathbf{k}) d\Omega d\mathbf{c}_e d\varepsilon. \end{aligned} \quad (A10)$$

In (A10),  $f$  with subscripts  $v$ ,  $e$ , and  $v - e$  refers to the probability density function for different kinds of particles

specified by their sizes (and velocities abbreviated). Symbols with “’” refer to the properties of reverse collisions.  $\mathbf{c}_{ev} = \mathbf{c}_\varepsilon - \mathbf{c}_v$  is the relative collision velocity between particles  $v$  and  $\varepsilon$  and  $\sigma$  is the interdistance of the two colliding particles referring to half of the addition of their diameters (of volume equivalent spheres).  $g_{ev}$  is the radial distribution function.<sup>7</sup>  $e_{ev}$  is given by  $\mathbf{c}'_{ev} = -e_{ev}\mathbf{c}_{ev}$ .  $\psi$  with subscripts specifies its value (the probability) for a particular collision to succeed for an aggregation.  $\chi$  is the Taylor's expansion when the sizes of two particles are taken into account in a collision to give the relative position of the two colliding particles.  $M_{v-\varepsilon}$  is the mass ratio between the mass of particle  $v - \varepsilon$ ,  $m_{v-\varepsilon}$ , and the addition of the masses ( $m_{v-\varepsilon} + m_\varepsilon$ ) of particles  $v - \varepsilon$  and  $\varepsilon$ , which means  $M_{v-\varepsilon} = m_{v-\varepsilon}/(m_{v-\varepsilon} + m_\varepsilon)$ .  $d\Omega$  is the differential angle multiplied by the square of a sphere radius to characterize the differential area of a spherical surface with  $\int \Omega d\Omega = \int_0^\pi \sin \omega d\omega \int_0^{2\pi} d\varphi = 4\pi$ , here  $\omega$  and  $\varphi$  represent the filling angles in spherical coordinates.

On the right hand side of (A10), the first term describes the net increase of particles  $v$  in terms of their velocity characteristic attributed to the forward and reverse collisions (without changing the number density  $n_v$  of the particles in their size  $v$ ). The second term gives the birth rate of the particles with regard to their size  $v$ , which is due to the completely inelastic collisions between particles  $\varepsilon$  and  $v - \varepsilon$ ; the third term shows the death rate of the particles  $v$  owing to the completely inelastic collisions between particles  $v$  and any sizes of particles. Together the second and third terms detail the net increase of particles  $v$  in terms of their size (number density  $n_v$  of the particles  $v$  has been changed).

The transport of the property  $\phi_v$  is calculated as  $\int \phi_v r_v d\mathbf{c}_v$  and given by (A11) as

$$\begin{aligned} & \frac{\partial(n_v \langle \phi_v \rangle)}{\partial t} + \frac{\partial}{\partial \mathbf{r}} \cdot n_v \langle \phi_v \mathbf{c}_v \rangle - n_v \left\langle \frac{\partial \phi_v}{\partial t} \right\rangle - n_v \left\langle \frac{\partial \phi_v}{\partial \mathbf{r}} \cdot \mathbf{c}_v \right\rangle \\ & - n_v \left\langle \frac{\partial \phi_v}{\partial \mathbf{c}_v} \cdot \frac{\mathbf{F}_v}{m_v} \right\rangle + \frac{\partial}{\partial v \mathbf{k}} \cdot n_v \langle \phi_v \mathbf{G}_v \rangle - \left\langle \frac{\partial \phi_v}{\partial v \mathbf{k}} \right\rangle \cdot n_v \mathbf{G}_v \\ & = \int \int \int \int (\phi'_v - \phi_v) (1 - \psi_{ev}) f_v f_\varepsilon \chi_{ev} g_{ev} \\ & \quad \times \frac{\sigma_{ev}^2}{4} (\mathbf{c}_{ev} \cdot \mathbf{k}) d\varepsilon d\Omega d\mathbf{c}_\varepsilon d\mathbf{c}_v \\ & + \int \int \int \int \phi_v \left[ \int_0^v \frac{1}{2M_{v-\varepsilon}^2} \psi_{\varepsilon, v-\varepsilon} f_{v-\varepsilon} f_\varepsilon \chi_{\varepsilon, v-\varepsilon} g_{\varepsilon, v-\varepsilon} \frac{\sigma_{\varepsilon, v-\varepsilon}^2}{4} (\mathbf{c}_{\varepsilon, v-\varepsilon} \cdot \mathbf{k}) d\varepsilon \right. \\ & \quad \left. - \int_0^\infty \psi_{ev} f_v f_\varepsilon \chi_{ev} g_{ev} \frac{\sigma_{ev}^2}{4} (\mathbf{c}_{ev} \cdot \mathbf{k}) d\varepsilon \right] d\Omega d\mathbf{c}_\varepsilon d\mathbf{c}_v. \quad (\text{A11}) \end{aligned}$$

As can be seen from the right hand side of (A11), the first term is the rate of net change of  $\phi_v$  contributed from the collisions with regard to the velocity characteristic of  $f_v$  (without changing  $n_v$ ); the second and third terms together give the rate of  $\phi_v$  attributed to the change of  $f_v$  in terms of its size characteristic (with  $n_v$  changed). Thus, according to (12), we have the following relations

$$\begin{aligned} n_v \Delta \langle \phi_v \rangle &= \int \int \int \int (\phi'_v - \phi_v) (1 - \psi_{ev}) f_v f_\varepsilon \chi_{ev} g_{ev} \\ & \quad \times \frac{\sigma_{ev}^2}{4} (\mathbf{c}_{ev} \cdot \mathbf{k}) d\varepsilon d\Omega d\mathbf{c}_\varepsilon d\mathbf{c}_v, \quad (\text{13a}) \end{aligned}$$

$$\begin{aligned} \langle \phi_v \rangle \Delta n_v &= \int \int \int \int \phi_v \left[ \int_0^v \frac{1}{2M_{v-\varepsilon}^2} \psi_{\varepsilon, v-\varepsilon} f_{v-\varepsilon} f_\varepsilon \chi_{\varepsilon, v-\varepsilon} g_{\varepsilon, v-\varepsilon} \right. \\ & \quad \left. \times \frac{\sigma_{\varepsilon, v-\varepsilon}^2}{4} (\mathbf{c}_{\varepsilon, v-\varepsilon} \cdot \mathbf{k}) d\varepsilon - \int_0^\infty \psi_{ev} f_v f_\varepsilon \chi_{ev} g_{ev} \frac{\sigma_{ev}^2}{4} (\mathbf{c}_{ev} \cdot \mathbf{k}) d\varepsilon \right] \\ & \quad d\Omega d\mathbf{c}_\varepsilon d\mathbf{c}_v. \quad (\text{13b}) \end{aligned}$$

As a simplified case for (A11), let  $\phi_v = 1$ , then  $\phi'_v = 1$ , also  $\psi_{ev} = 0$  (without aggregation of particles) and  $\mathbf{G}_v = 0$  (without molecular deposition for particles' growth), (A11) becomes  $\frac{\partial n_v}{\partial t} + \frac{\partial}{\partial \mathbf{r}} \cdot n_v \mathbf{u}_v = 0$ , multiplying both sides of it by  $v$  and integrating over  $v$  space, we then have  $\frac{\partial \varepsilon_s}{\partial t} + \frac{\partial}{\partial \mathbf{r}} \cdot \varepsilon_s \mathbf{u}_s = 0$ . These are the typical continuity equations in multiple phase flow<sup>27</sup> without the change of particle size and number density taking place.

However, with  $\psi_{ev} \neq 0$  and  $\phi_v$  becoming more complicated such as  $m_v \mathbf{c}_v$  and  $m_v c_v^2/2$ , evaluation of (13a–b), that is, the right hand side of (A11), becomes necessary and is presented in the next section for deriving the kinetic transport equations. It is worth noting at this stage that the transport equations for continuity, momentum and kinetic energy for all the particles, the conservation of mass and momentum needs to be proven and the dissipation of the kinetic energy needs to be given because  $\psi_{ev} \neq 0$  and the restitution of coefficient  $e_{ev}$  are involved in the evaluation, that is, either (13a), (13b) or both not equal to 0 thus require detailed calculation.

## Kinetic Transport Equations

To generate the kinetic transport equations, that is, to evaluate (13a) and (13b), it is necessary to know the mathematical form of  $f_v$ . As indicated in (1), the following approximation is made

$$f_v = f(v, \mathbf{c}_v, \mathbf{r}, t) \cong n(v, \mathbf{r}, t) \lambda(\mathbf{c}_v, \mathbf{r}, t) = n_v \lambda_v, \quad (\text{14})$$

where  $\lambda(\mathbf{c}_v, \mathbf{r}, t) = \lambda_v$  and is corresponding to the normalized velocity distribution function of particles  $v$ . This approximation suggests a mutually independent behavior between the particle size and velocity expressed in  $f_v$ . Thus,  $\lambda_v$  implies the probability of the particles with size  $v$  appearing to have velocity  $\mathbf{c}_v$ . According to Assumption 3,  $\lambda_v$  takes the form of Maxwell's distribution, we then have

$$f_v = n_v \left( \frac{m_v}{2\pi\theta_s} \right)^{\frac{3}{2}} \exp \left[ -\frac{m_v (\mathbf{c}_v - \mathbf{u}_s)^2}{2\theta_s} \right], \quad (\text{15a})$$

where  $\theta_s$  is the mixture granular energy defined in (8). It is worth pointing out that this function can be extended to higher orders according to Chapman-Enskog's approximation<sup>7</sup> but it has captured the main features of the distribution of the particles in terms of their velocity. According to (6) for the fluctuation velocity of particles, (15a) becomes

$$f_v = n_v \left( \frac{m_v}{2\pi\theta_s} \right)^{\frac{3}{2}} \exp \left[ -\frac{m_v C_v^2}{2\theta_s} \right]. \quad (\text{15b})$$

Taking the 0th order of  $\chi_{ev}$  (means relatively dilute systems, the distance of particles to travel for a collision is much greater than the sizes of the particles), that is,  $\chi_{ev} = 1$ , (A11) is



changed to

$$\begin{aligned}
& \frac{\partial(n_v \langle \phi_v \rangle)}{\partial t} + \frac{\partial}{\partial \mathbf{r}} \cdot n_v \langle \phi_v \mathbf{c}_v \rangle - n_v \left\langle \frac{\partial \phi_v}{\partial t} \right\rangle - n_v \left\langle \frac{\partial \phi_v}{\partial \mathbf{r}} \cdot \mathbf{c}_v \right\rangle \\
& - n_v \left\langle \frac{\partial \phi_v}{\partial \mathbf{c}_v} \cdot \frac{\mathbf{F}_v}{m_v} \right\rangle + \frac{\partial}{\partial \mathbf{v} \mathbf{k}} \cdot n_v \langle \phi_v \mathbf{G}_v \rangle - \left\langle \frac{\partial \phi_v}{\partial \mathbf{v} \mathbf{k}} \right\rangle \cdot n_v \mathbf{G}_v \\
& = n_v \int_0^\infty n_e g_{ev} \frac{\sigma_{ev}^2}{4} \iiint (\phi_v' - \phi_v) (1 - \psi_{ev}) \\
& \quad \times \lambda_v \lambda_e (\mathbf{C}_{ev} \cdot \mathbf{k}) d\Omega d\mathbf{C}_e d\mathbf{C}_v d\epsilon \\
& \quad + \int_0^v \frac{1}{2M_{v-\epsilon}^2} \psi_{e,v-\epsilon} n_{v-\epsilon} n_e g_{e,v-\epsilon} \\
& \quad \times \frac{\sigma_{e,v-\epsilon}^2}{4} \iiint \phi_v \lambda_{v-\epsilon} \lambda_e (\mathbf{C}_{ev} \cdot \mathbf{k}) d\Omega d\mathbf{C}_e d\mathbf{C}_v d\epsilon \\
& - n_v \int_0^\infty \psi_{ev} n_e g_{ev} \frac{\sigma_{ev}^2}{4} \iiint \phi_v \lambda_v \lambda_e (\mathbf{C}_{ev} \cdot \mathbf{k}) d\Omega d\mathbf{C}_e d\mathbf{C}_v d\epsilon. \quad (16)
\end{aligned}$$

The above transformation is carried out with  $f(\mathbf{c}_v, v, \mathbf{r}, t)$   $d\mathbf{c}_v = f(\mathbf{C}_v, v, \mathbf{r}, t) d\mathbf{C}_v$  and

$$\lambda_v \lambda_e (\mathbf{c}_{ev} \cdot \mathbf{k}) d\Omega d\mathbf{c}_v d\mathbf{c}_e = \lambda_v \lambda_e (\mathbf{C}_{ev} \cdot \mathbf{k}) d\Omega d\mathbf{C}_v d\mathbf{C}_e, \quad (17)$$

where  $\mathbf{C}_{ev} = \mathbf{C}_e - \mathbf{C}_v$  is the relative fluctuation velocity. Additionally,  $d\mathbf{C}_v d\mathbf{C}_e$  can be changed to the form of  $d\mathbf{C}_c d\mathbf{C}_{ev}$  ( $\mathbf{C}_c$  is the mass center velocity of particles  $v$  and  $e$  as defined similarly to that in (A9)) with

$$d\mathbf{C}_v d\mathbf{C}_e = \left| \frac{\partial(\mathbf{C}_v, \mathbf{C}_e)}{\partial(\mathbf{C}_c, \mathbf{C}_{ev})} \right| d\mathbf{C}_c d\mathbf{C}_{ev} = d\mathbf{C}_c d\mathbf{C}_{ev}, \quad (18)$$

and the following expressions<sup>7</sup>

$$\begin{aligned}
d\mathbf{C}_{ev} &= (d\mathbf{C}_{ev})_x (d\mathbf{C}_{ev})_y (d\mathbf{C}_{ev})_z = C_{ev}^2 d\mathbf{C}_{ev} d\Omega, \\
d\mathbf{C}_c &= C_c^2 d\mathbf{C}_c d\Omega, d\mathbf{C}_{ev} d\mathbf{C}_c = C_{ev}^2 d\mathbf{C}_{ev} d\Omega C_c^2 d\mathbf{C}_c d\Omega. \quad (19)
\end{aligned}$$

### The continuity equations

The continuity equation for the number density  $n_v$  of particles  $v$  can be obtained from (16) by letting  $\phi_v = 1$ , then  $\phi_v' = 1$  as follows

$$\begin{aligned}
& \frac{\partial n_v}{\partial t} + \frac{\partial}{\partial \mathbf{r}} \cdot n_v \mathbf{u}_v + \frac{\partial}{\partial \mathbf{v} \mathbf{k}} \cdot n_v \mathbf{G}_v = \int_0^v \frac{1}{2M_{v-\epsilon}^2} \psi_{e,v-\epsilon} n_{v-\epsilon} n_e g_{e,v-\epsilon} \\
& \quad \times \frac{\sigma_{e,v-\epsilon}^2}{4} d\epsilon \iiint \lambda_{v-\epsilon} \lambda_e (\mathbf{C}_{ev} \cdot \mathbf{k}) d\Omega d\mathbf{C}_e d\mathbf{C}_v \\
& - n_v \int_0^\infty \psi_{ev} n_e g_{ev} \frac{\sigma_{ev}^2}{4} d\epsilon \iiint \lambda_v \lambda_e (\mathbf{C}_{ev} \cdot \mathbf{k}) d\Omega d\mathbf{C}_e d\mathbf{C}_v. \quad (20)
\end{aligned}$$

On the right hand side of (20), the triple integrations of the normalized Maxwell's velocity distribution functions  $\lambda_{v-\epsilon}$ ,  $\lambda_e$  and  $\lambda_v$  over the domains of  $\Omega$ ,  $\mathbf{C}_e$ , and  $\mathbf{C}_v$  can be calculated according to (18) and (19) for the values of  $\mathbf{C}_c$  and  $\mathbf{C}_{ev}$  ranging from 0 to  $\infty$ ; (20) thus becomes

$$\begin{aligned}
& \frac{\partial n_v}{\partial t} + \frac{\partial}{\partial \mathbf{r}} \cdot n_v \mathbf{u}_v + \frac{\partial}{\partial \mathbf{v} \mathbf{k}} \cdot n_v \mathbf{G}_v = \frac{1}{2} \int_0^v \left[ \frac{8\pi\theta_s(m_{v-\epsilon} + m_e)}{m_{v-\epsilon} m_e} \right]^{\frac{1}{2}} \\
& \quad \times \psi_{e,v-\epsilon} g_{e,v-\epsilon} \sigma_{e,v-\epsilon}^2 n_{v-\epsilon} n_e d\epsilon - n_v \int_0^\infty \left[ \frac{8\pi\theta_s(m_v + m_e)}{m_v m_e} \right]^{\frac{1}{2}} \\
& \quad \times \psi_{ev} g_{ev} \sigma_{ev}^2 n_e d\epsilon. \quad (21)
\end{aligned}$$

This is the standard population balance equation<sup>46,50-53</sup> in the form of aggregation and growth and has been widely used in the modeling and simulation of engineering particulate systems<sup>54,55</sup> to predict the particle size distributions<sup>51,53</sup> when size enlargement events occurred.

Equation 21 has some interesting features presented as the following. Let  $\xi(v)$  be a property of size  $v$ , multiply it to both sides of (21) then integrate the equation over  $v$  in the domain  $(0, \infty)$ , also according to (9a) for  $\mathbf{u}_v = \mathbf{u}_s + \mathbf{w}_v$ , we have

$$\begin{aligned}
& \int_0^\infty \xi(v) \frac{\partial n_v}{\partial t} dv + \int_0^\infty \xi(v) \frac{\partial}{\partial \mathbf{r}} \cdot n_v (\mathbf{u}_s + \mathbf{w}_v) dv \\
& \quad + \int_0^\infty \xi(v) \frac{\partial}{\partial \mathbf{v} \mathbf{k}} \cdot n_v \mathbf{G}_v dv \\
& = \frac{1}{2} \int_0^\infty \int_0^\infty \xi(v) \left[ \frac{8\pi\theta_s(m_\zeta + m_e)}{m_\zeta m_e} \right]^{\frac{1}{2}} \psi_{e\zeta} g_{e\zeta} \sigma_{e\zeta}^2 n_\zeta n_e d\zeta d\epsilon \\
& - \int_0^\infty \int_0^\infty \xi(v) \left[ \frac{8\pi\theta_s(m_v + m_e)}{m_v m_e} \right]^{\frac{1}{2}} \psi_{ev} g_{ev} \sigma_{ev}^2 n_v n_e d\epsilon dv. \quad (22)
\end{aligned}$$

The first term on the right hand side of (22) is obtained by exchanging the order of the integrations for  $v - \epsilon$  and  $\epsilon$  and then letting  $\zeta = v - \epsilon$  thus  $\zeta \in (0, \infty)$ .

Replacing  $\xi(v)$  with 1 in (22), according to (2a) and (9c), the continuity equation for the total number of particles is

$$\begin{aligned}
& \frac{\partial N}{\partial t} + \frac{\partial}{\partial \mathbf{r}} \cdot N(\mathbf{u}_s + \mathbf{w}_s) = -\frac{1}{2} \int_0^\infty \int_0^\infty \left[ \frac{8\pi\theta_s(m_v + m_e)}{m_v m_e} \right]^{\frac{1}{2}} \\
& \quad \times \psi_{ev} g_{ev} \sigma_{ev}^2 n_v n_e d\epsilon dv. \quad (23a)
\end{aligned}$$

In (23a), the term  $\int_0^\infty \frac{\partial}{\partial \mathbf{v} \mathbf{k}} \cdot n_v \mathbf{G}_v dv = 0$  is due to the fact that  $n_v \mathbf{G}_v \rightarrow 0$  as particle size  $v \rightarrow 0$  and  $\infty$ . Note in this equation, the convective flux is with velocity  $\mathbf{u}_s + \mathbf{w}_s$  as  $\mathbf{u}_s$  is the particles volume fraction weighted bulk velocity instead of number weighted thus the number weighted diffusion velocity  $\mathbf{w}_s$  is generated as an extra term. It is worth pointing out that (23a) explains the decrease of the total number of particles in a quantitative way for the systems where aggregation takes place.

Similarly, let  $\xi(v) = v$  and  $m_v$  [note,  $v = v - \epsilon + \epsilon = \zeta + \epsilon$  and  $m_v = m_{v-\epsilon} + m_e = m_\zeta + m_e$  the right hand of (22) is equal to 0], the continuity equations for the volume fraction and mass density of all particles according to (2b), (2c),  $\partial v / \partial t = 0$ ,  $\partial v / \partial \mathbf{r} = 0$ ,  $\partial m_v / \partial t = 0$  and  $\partial m_v / \partial \mathbf{r} = 0$  are

$$\frac{\partial \epsilon_s}{\partial t} + \frac{\partial}{\partial \mathbf{r}} \cdot \epsilon_s \mathbf{u}_s = 0, \quad (23b)$$

$$\frac{\partial(\epsilon_s \rho_s)}{\partial t} + \frac{\partial}{\partial \mathbf{r}} \cdot (\epsilon_s \rho_s \mathbf{u}_s) = 0. \quad (23c)$$

Equations 23b and 23c demonstrate the conservation of the total volume and mass of particles, respectively, for the aggregation of particles in granular flow systems.

## The momentum equations

Similar to generating the continuity equations, the establishment of momentum and granular energy equations is as well for both the particles with a specific size  $v$  and all the particles in the system. The purpose to establish the equations for all the particles is to prove the conservativity (total momentum) and dissipativity (total kinetic energy) of the particles in the case of aggregation; and in particular to calculate the dissipation of the total kinetic energy due to the inelastic collisions and aggregation of particles.

For the momentum equation of particles  $v$ , by letting  $\phi_v = m_v \mathbf{c}_v$ , after the collisions with particles  $\varepsilon$ , the momentum of particles  $v$  is changed to  $\phi'_v = m_v \mathbf{c}'_v$ , thus we obtain

$$\phi'_v - \phi_v = m_v(\mathbf{c}'_v - \mathbf{c}_v) = m_v M_\varepsilon(1 + e_{\varepsilon v})\mathbf{C}_{\varepsilon v}, \quad (24)$$

which is due to  $\mathbf{c}_v = \mathbf{c}_c - M_\varepsilon \mathbf{c}_{\varepsilon v}$ ,  $\mathbf{c}'_v = \mathbf{c}_c - M_\varepsilon \mathbf{c}'_{\varepsilon v}$ ,  $\mathbf{c}_c = \mathbf{C}_c$ ,  $\mathbf{c}_{\varepsilon v} = \mathbf{C}_{\varepsilon v}$ ,  $\mathbf{c}'_{\varepsilon v} = \mathbf{C}'_{\varepsilon v}$  and  $\mathbf{C}_{\varepsilon v} = -e_{\varepsilon v} \mathbf{C}'_{\varepsilon v}$ . Then, the momentum equation for particles  $v$  according to (16),  $\partial \mathbf{c}_v / \partial t = 0$ ,  $\partial \mathbf{c}_v / \partial \mathbf{r} = 0$  and  $\partial \mathbf{C}_v / \partial \mathbf{r} = 0$  ( $\mathbf{c}_v$  and  $\mathbf{C}_v$  are not the functions of  $\mathbf{r}$  and  $t$ ) is

$$\begin{aligned} & \frac{\partial(n_v m_v \mathbf{u}_v)}{\partial t} + \frac{\partial}{\partial \mathbf{r}} \cdot [n_v m_v \mathbf{u}_s(\mathbf{u}_v + \mathbf{w}_v)] + \frac{\partial}{\partial v \mathbf{k}} \cdot (n_v m_v \mathbf{u}_v \mathbf{G}_v) \\ & + \frac{\partial P_v}{\partial \mathbf{r}} + \frac{\partial}{\partial \mathbf{r}} \cdot \bar{\mathbf{r}}_v - n_v \langle \mathbf{F}_v \rangle \\ & = n_v \int_0^\infty n_\varepsilon (1 - \psi_{\varepsilon v})(1 + e_{\varepsilon v}) g_{\varepsilon v} 3\pi \theta_s \sigma_{\varepsilon v}^2 \mathbf{k} d\varepsilon \\ & + \int_0^v n_{v-\varepsilon} n_\varepsilon \psi_{\varepsilon, v-\varepsilon} g_{\varepsilon, v-\varepsilon} \sigma_{\varepsilon, v-\varepsilon}^2 \left\{ \frac{4\theta_s m_v \mathbf{k}}{(m_{v-\varepsilon} m_\varepsilon)^{\frac{1}{2}}} \right. \\ & \quad \left. + m_v \mathbf{u}_s \left[ \frac{2\pi \theta_s (m_{v-\varepsilon} + m_\varepsilon)^{\frac{1}{2}}}{m_{v-\varepsilon} m_\varepsilon} \right] \right\} d\varepsilon \\ & - n_v \int_0^\infty n_\varepsilon \psi_{\varepsilon v} g_{\varepsilon v} \sigma_{\varepsilon v}^2 \left\{ \theta_s \left( 8\sqrt{\frac{m_v}{m_\varepsilon}} - 3\pi \right) \mathbf{k} \right. \\ & \quad \left. + \mathbf{u}_s \left[ \frac{8\pi \theta_s (m_v + m_\varepsilon) m_v}{m_\varepsilon} \right]^{\frac{1}{2}} \right\} d\varepsilon, \quad (25) \end{aligned}$$

where  $P_v$  and  $\bar{\mathbf{r}}_v$  are the normal solid pressure and stress tensor of particles  $v$ , respectively.

$$P_v = n_v m_v \langle (\mathbf{C}_v)_i (\mathbf{C}_v)_i \rangle, \quad (26a)$$

$$\bar{\mathbf{r}}_v = n_v m_v \langle (\mathbf{C}_v)_i (\mathbf{C}_v)_j \rangle_{i \neq j}. \quad (26b)$$

Equation 25 essentially explains all the forces that are imposed on particles  $v$ , causing the change of the momentum of these particles as a whole in time, spatial, and size coordinates. The change of the momentum of particles  $v$  is thus attributed to the external force  $\mathbf{F}_v$ , collisions that particles  $v$  encountered [the first term of the right hand side of (25)] and the net change of the number of particles  $v$  owing to aggregation [the second and third terms of the right hand side of (25)].

The total momentum of particles can be obtained by integrating both sides of (25) over  $v$  domain  $(0, \infty)$ , the left hand side of this equation thus becomes

$$\frac{\partial(\varepsilon_s \rho_s \mathbf{u}_s)}{\partial t} + \frac{\partial}{\partial \mathbf{r}} \cdot (\varepsilon_s \rho_s \mathbf{u}_s \mathbf{u}_s) + \frac{\partial P_s}{\partial \mathbf{r}} + \frac{\partial}{\partial \mathbf{r}} \cdot \bar{\mathbf{r}}_s - N \langle \mathbf{F}_v \rangle, \quad (27)$$

where the transformation is made according to (2c), (5), (9b),  $\int_0^\infty P_v dv = P_s$  and  $\int_0^\infty \bar{\mathbf{r}}_v dv = \bar{\mathbf{r}}_s$ .

To obtain the integrated terms on the right hand side of (38), it is necessary to trace back (16). For the first term of the right hand side of (16), as  $\phi'_v - \phi_v = m_v(\mathbf{c}'_v - \mathbf{c}_v)$  and the integration over the entire domain of size  $v$  is being made, it then represents the change of the total momentum of particles  $v$  and  $\varepsilon$  due to all the collisions between them. This term can thus be written as

$$\begin{aligned} & \int_0^\infty n_v \int_0^\infty n_\varepsilon g_{\varepsilon v} \frac{\sigma_{\varepsilon v}^2}{4} \iiint m_v(\mathbf{c}'_v - \mathbf{c}_v)(1 - \psi_{\varepsilon v}) \lambda_v \lambda_\varepsilon \\ & \times (\mathbf{C}_{\varepsilon v} \cdot \mathbf{k}) d\Omega d\mathbf{C}_\varepsilon d\mathbf{C}_v d\varepsilon dv = \frac{1}{2} \int_0^\infty n_v \int_0^\infty n_\varepsilon g_{\varepsilon v} \frac{\sigma_{\varepsilon v}^2}{4} \\ & \times \iiint (m_v \mathbf{c}'_v - m_v \mathbf{c}_v + m_\varepsilon \mathbf{c}'_\varepsilon - m_\varepsilon \mathbf{c}_\varepsilon) \\ & \times (1 - \psi_{\varepsilon v}) \lambda_v \lambda_\varepsilon (\mathbf{C}_{\varepsilon v} \cdot \mathbf{k}) d\Omega d\mathbf{C}_\varepsilon d\mathbf{C}_v d\varepsilon dv, \quad (28) \end{aligned}$$

which is equal to 0 as  $m_v \mathbf{c}_v + m_\varepsilon \mathbf{c}_\varepsilon = m_v \mathbf{c}'_v + m_\varepsilon \mathbf{c}'_\varepsilon$ .

With  $\phi_v = m_v \mathbf{c}_v$  and  $m_v = m_{v-\varepsilon} + m_\varepsilon$ , the second term of the right hand side of (16) after integration over  $v$  domain becomes

$$\begin{aligned} & \int_0^\infty \int_0^v \frac{1}{2M_{v-\varepsilon}^2} \psi_{\varepsilon, v-\varepsilon} n_{v-\varepsilon} n_\varepsilon g_{\varepsilon, v-\varepsilon} \frac{\sigma_{\varepsilon, v-\varepsilon}^2}{4} \\ & \times \iiint m_v \mathbf{c}_v \lambda_{v-\varepsilon} \lambda_\varepsilon (\mathbf{C}_{\varepsilon v} \cdot \mathbf{k}) d\Omega d\mathbf{C}_\varepsilon d\mathbf{C}_v d\varepsilon dv \\ & = \int_0^\infty \int_0^v \frac{1}{2} \psi_{\varepsilon, v-\varepsilon} n_{v-\varepsilon} n_\varepsilon g_{\varepsilon, v-\varepsilon} \frac{\sigma_{\varepsilon, v-\varepsilon}^2}{4} \iiint (m_{v-\varepsilon} \mathbf{c}_{v-\varepsilon} \\ & + m_\varepsilon \mathbf{c}_\varepsilon) \lambda_{v-\varepsilon} \lambda_\varepsilon (\mathbf{C}_{\varepsilon, v-\varepsilon} \cdot \mathbf{k}) d\Omega d\mathbf{C}_\varepsilon d\mathbf{C}_{v-\varepsilon} d\varepsilon dv, \quad (29) \end{aligned}$$

in which  $m_v \mathbf{c}_v = m_\varepsilon \mathbf{c}_\varepsilon + m_{v-\varepsilon} \mathbf{c}_{v-\varepsilon}$  is due to the fact that  $\mathbf{c}_v$  is the mass center velocity of particles  $\varepsilon$  and  $v - \varepsilon$  as expressed in (A9). Similar treatment to that in (22) by exchanging the order of the integrations for  $\varepsilon$  and  $v$  and letting  $v - \varepsilon = \zeta$  transforms (29) into

$$\begin{aligned} & \int_0^\infty \int_\varepsilon^\infty \frac{1}{2} \psi_{\varepsilon, v-\varepsilon} n_{v-\varepsilon} n_\varepsilon g_{\varepsilon, v-\varepsilon} \frac{\sigma_{\varepsilon, v-\varepsilon}^2}{4} \\ & \times \iiint (m_{v-\varepsilon} \mathbf{c}_{v-\varepsilon} + m_\varepsilon \mathbf{c}_\varepsilon) \lambda_{v-\varepsilon} \lambda_\varepsilon (\mathbf{C}_{\varepsilon, v-\varepsilon} \cdot \mathbf{k}) d\Omega d\mathbf{C}_\varepsilon d\mathbf{C}_{v-\varepsilon} dv d\varepsilon \\ & = \int_0^\infty \int_0^\infty \frac{1}{2} \psi_{\varepsilon, v-\varepsilon} n_{v-\varepsilon} n_\varepsilon g_{\varepsilon, v-\varepsilon} \frac{\sigma_{\varepsilon, v-\varepsilon}^2}{4} \\ & \times \iiint (m_{v-\varepsilon} \mathbf{c}_{v-\varepsilon} + m_\varepsilon \mathbf{c}_\varepsilon) \lambda_{v-\varepsilon} \lambda_\varepsilon \\ & \times (\mathbf{C}_{\varepsilon, v-\varepsilon} \cdot \mathbf{k}) d\Omega d\mathbf{C}_\varepsilon d\mathbf{C}_{v-\varepsilon} d(v - \varepsilon) d\varepsilon \\ & = \int_0^\infty \int_0^\infty \frac{1}{2} \psi_{\varepsilon, \zeta} n_\zeta n_\varepsilon g_{\varepsilon, \zeta} \frac{\sigma_{\varepsilon, \zeta}^2}{4} \iiint (m_\zeta \mathbf{c}_\zeta + m_\varepsilon \mathbf{c}_\varepsilon) \\ & \times \lambda_\zeta \lambda_\varepsilon (\mathbf{C}_{\varepsilon, \zeta} \cdot \mathbf{k}) d\Omega d\mathbf{C}_\varepsilon d\mathbf{C}_\zeta d\zeta d\varepsilon. \quad (30) \end{aligned}$$

As particles  $\zeta$  and  $\varepsilon$  in (30) are indistinguished and the integrations over their entire domains are being carried out, (30) can be written as

$$\int_0^\infty \int_0^\infty \psi_{e,v} n_v n_e g_{e,v} \frac{\sigma_{e,v}^2}{4} \iiint m_v \mathbf{c}_v \lambda_v \lambda_e (\mathbf{C}_{e,v} \cdot \mathbf{k}) \times d\Omega d\mathbf{C}_v d\mathbf{C}_v dv d\epsilon, \quad (30)$$

which is essentially the same as the integration of the third term of the right hand side of (16) over  $v$  domain with  $\phi_v = m_v \mathbf{c}_v$ . Thus, the second and the third terms of the right hand side of (16) after the integration over  $v$  with  $\phi_v = m_v \mathbf{c}_v$  are cancelled. The momentum equation for all the particles taking (27) forward hence becomes

$$\frac{\partial(\epsilon_s \rho_s \mathbf{u}_s)}{\partial t} + \frac{\partial}{\partial \mathbf{r}} \cdot (\epsilon_s \rho_s \mathbf{u}_s \mathbf{u}_s) + \frac{\partial P_s}{\partial \mathbf{r}} + \frac{\partial}{\partial \mathbf{r}} \cdot \bar{\boldsymbol{\tau}}_s - N \langle \mathbf{F}_v \rangle = 0. \quad (32)$$

This has given a detailed mathematical proof for the conservation of the total momentum of all the particles in a system when aggregation occurs.

### The granular energy equations

The granular energy equation of particles  $v$  can be obtained by replacing  $\phi_v$  with  $m_v c_v^2/2$  into (16). Because the granular energy is defined with fluctuation velocity as expressed in (7) and by carrying out the integration for the right hand side of (16) for  $\phi_v = m_v c_v^2/2$ , for particles  $v$ , their granular energy equation becomes

$$\begin{aligned} & \frac{3}{2} \left[ \frac{\partial(n_v \theta_v)}{\partial t} + \frac{\partial}{\partial \mathbf{r}} \cdot (n_v \theta_v \mathbf{u}_s) \right] \\ & + \frac{1}{2} \left\{ \frac{\partial(n_v m_v u_s^2)}{\partial t} + \frac{\partial}{\partial \mathbf{r}} \cdot [n_v m_v u_s^2 (\mathbf{u}_v + \mathbf{w}_v)] \right\} \\ & + \left\{ \frac{\partial[n_v m_v (\mathbf{u}_s \cdot \mathbf{w}_v)]}{\partial t} + \frac{\partial}{\partial \mathbf{r}} \cdot [n_v m_v (\mathbf{u}_s \cdot \mathbf{w}_v) \cdot \mathbf{u}_s] \right\} + \frac{\partial}{\partial \mathbf{r}} \cdot \mathbf{q}_v \\ & + P_v \frac{\partial}{\partial \mathbf{r}} \cdot \mathbf{u}_s + \bar{\boldsymbol{\tau}}_v : \frac{\partial}{\partial \mathbf{r}} \mathbf{u}_s + \frac{3}{2} \frac{\partial}{\partial v \mathbf{k}} \cdot (n_v \theta_v \mathbf{G}_v) \\ & - n_v m_v \langle (\mathbf{C}_v + \mathbf{u}_s) \cdot \mathbf{F}_v \rangle = n_v \int_0^\infty n_e (1 - \psi_{ev}) g_{ev} \sigma_{ev}^2 \\ & \times \left\{ \frac{2\sqrt{2}\pi\theta_s^3 (1 + e_{ev}) m_e^{\frac{1}{2}}}{(m_v + m_e)^{\frac{1}{2}}} \left[ \frac{2(e_{ev} - 1)}{m_v^{\frac{1}{2}}} + \frac{3}{m_e^{\frac{1}{2}}} \right] \right. \\ & + 3\pi\theta_s (1 + e_{ev}) (\mathbf{u}_s \cdot \mathbf{k}) \left. \right\} d\epsilon + \int_0^v n_{v-\epsilon} n_e \psi_{e,v-\epsilon} g_{e,v-\epsilon} \sigma_{e,v-\epsilon}^2 m_v \\ & \times \left\{ \frac{3\sqrt{2}\pi\theta_s^3}{2(m_e + m_{v-\epsilon})^{\frac{1}{2}} (m_e m_{v-\epsilon})^{\frac{1}{2}}} + \left[ \frac{\pi\theta_s (m_e + m_{v-\epsilon})}{2m_e m_{v-\epsilon}} \right]^{\frac{1}{2}} \right. \\ & \times u_s^2 \frac{4\pi\theta_s (\mathbf{u} \cdot \mathbf{k})}{(m_e m_{v-\epsilon})^{\frac{1}{2}}} \left. \right\} d\epsilon - n_v \int_0^\infty n_e \psi_{ev} g_{ev} \sigma_{ev}^2 \\ & \times \left\{ \frac{\sqrt{2}\pi\theta_s^3}{(m_e + m_v)^{\frac{1}{2}}} \left[ 3 \left( \frac{m_v}{m_e} \right)^{\frac{1}{2}} + 8 \left( \frac{m_e}{m_v} \right)^{\frac{1}{2}} - 6 \right] + 8\theta_s (\mathbf{u}_s \cdot \mathbf{k}) \left( \frac{m_v}{m_e} \right)^{\frac{1}{2}} \right. \\ & \left. - 3\pi\theta_s (\mathbf{u}_s \cdot \mathbf{k}) + m_v u_s^2 \left[ \frac{2\pi\theta_s (m_e + m_{v-\epsilon})}{m_e m_v} \right]^{\frac{1}{2}} \right\} d\epsilon, \quad (33) \end{aligned}$$

where  $\mathbf{q}_v$  is the heat flux defined as  $\mathbf{q}_v = n_v m_v \langle C_v^2 \mathbf{C}_v \rangle / 2$ .

As the property being transported is the actual kinetic energy ( $m_v c_v^2/2$ ) but  $\theta_v$  is related to the dot product of  $\mathbf{C}_v$

( $\langle \mathbf{C}_v \cdot \mathbf{C}_v \rangle$ ) with also  $\mathbf{c}_v = \mathbf{C}_v + \mathbf{u}_s$ , it is thus seen that on the left hand side of (33), two extra total differential terms are generated with respect to the bulk velocity  $\mathbf{u}_s$ . They are explained as follows.

The second group (two terms with  $u_s^2$  in  $\{\}$ ) describes the transfer of the kinetic energy of particles  $v$  moving as a whole with all other particles; the third group (two terms with  $(\mathbf{u}_s \cdot \mathbf{w}_v)$  in  $\{\}$ ) is understood as the transfer of the kinetic energy of particles  $v$  due to their diffusion with a velocity  $\mathbf{w}_v$  relative to the bulk particles with the ensemble average velocity  $\mathbf{u}_s$ .

The physical meanings of other terms on the left hand side of (33) are similar to that explained in the works of Davidson and Harrison,<sup>56</sup> Kunii and Levenspiel,<sup>57</sup> and Gidaspow.<sup>27</sup>

The mixture granular energy of all particles can then be generated by integrating both sides of (33) over particle size domain  $(0, \infty)$ ; thus the left hand side of (33) becomes

$$\begin{aligned} & \frac{3}{2} \left[ \frac{\partial(N\theta_s)}{\partial t} + \frac{\partial}{\partial \mathbf{r}} \cdot (N\theta_s \mathbf{u}_s) \right] + \frac{1}{2} \left[ \frac{\partial(\epsilon_s \rho_s u_s^2)}{\partial t} + \frac{\partial}{\partial \mathbf{r}} \cdot (\epsilon_s \rho_s u_s^2 \mathbf{u}_s) \right] \\ & + \frac{\partial}{\partial \mathbf{r}} \cdot \mathbf{q}_s + P_s \frac{\partial}{\partial \mathbf{r}} \cdot \mathbf{u}_s + \bar{\boldsymbol{\tau}}_s : \frac{\partial}{\partial \mathbf{r}} \mathbf{u}_s - \epsilon_s \rho_s \langle (\mathbf{C}_v + \mathbf{u}_s) \cdot \mathbf{F}_v \rangle, \quad (34) \end{aligned}$$

where  $\mathbf{q}_s = \int_0^\infty \mathbf{q}_v dv$ ,  $n_v \theta_v \mathbf{G}_v$ , converges with  $v \rightarrow 0$  and  $\infty$ ; and the terms with the dot product of diffusion velocity  $\mathbf{w}_v$  after integration are equal to 0 according to (9b).

For the integration of the right hand side of (33) over  $v$ , considering the terms of the right hand side of (16), a similar treatment can be made as to that for the total momentum equation of all particles. Therefore, the kinetic energy dissipation due to the inelastic collisions,  $\Delta E_c$ , the first term of the right hand side of (16) for  $\phi_v = m_v c_v^2/2$ , with the integrations over  $v$  and  $\epsilon$  from 0 to  $\infty$  being carried out, which indicates particles  $v$  and  $\epsilon$  are indistinguishable, becomes

$$\begin{aligned} \Delta E_c &= \int_0^\infty n_v \int_0^\infty n_e g_{ev} \frac{\sigma_{ev}^2}{4} \iiint \frac{1}{2} m_v (c_v'^2 - c_v^2) (1 - \psi_{ev}) \\ & \times \lambda_v \lambda_e (\mathbf{C}_{ev} \cdot \mathbf{k}) d\Omega d\mathbf{C}_e d\mathbf{C}_v d\epsilon dv = \frac{1}{4} \int_0^\infty n_v \int_0^\infty n_e g_{ev} \\ & \times \frac{\sigma_{ev}^2}{4} \iiint (m_v c_v'^2 - m_v c_v^2 + m_e c_e'^2 - m_e c_e^2) (1 - \psi_{ev}) \\ & \times \lambda_v \lambda_e (\mathbf{C}_{ev} \cdot \mathbf{k}) d\Omega d\mathbf{C}_e d\mathbf{C}_v d\epsilon dv \\ & = \int_0^\infty n_v \int_0^\infty n_e (1 - \psi_{ev}) g_{ev} \sigma_{ev}^2 (e_{ev}'^2 - 1) \\ & \times \left[ \frac{8\pi\theta_s^3 (m_e + m_v)}{m_e m_v} \right]^{\frac{1}{2}} d\epsilon dv. \quad (35) \end{aligned}$$

As can be seen in (35), because  $e_{ev} \leq 1$  and  $\psi_{ev} \leq 1$ , then  $\Delta E_c \leq 0$ .

The second term of the right hand side of (16) for  $\phi_v = m_v c_v^2/2$  with also the integration over  $v$  becomes

$$\begin{aligned}
& \int_0^\infty \int_0^v \frac{1}{2M_{v-\varepsilon}^2} \psi_{\varepsilon, v-\varepsilon} n_{v-\varepsilon} n_{\varepsilon} g_{\varepsilon, v-\varepsilon} \frac{\sigma_{\varepsilon, v-\varepsilon}^2}{4} \iiint \frac{1}{2} m_v c_v^2 \lambda_{v-\varepsilon} \lambda_{\varepsilon} (\mathbf{C}_{\varepsilon v} \cdot \mathbf{k}) d\Omega d\mathbf{C}_{\varepsilon} d\mathbf{C}_v d\varepsilon dv \\
&= \int_0^\infty \int_0^v \frac{1}{2} \psi_{\varepsilon, v-\varepsilon} n_{v-\varepsilon} n_{\varepsilon} g_{\varepsilon, v-\varepsilon} \frac{\sigma_{\varepsilon, v-\varepsilon}^2}{4} \iiint \frac{1}{2} (m_{v-\varepsilon} + m_{\varepsilon}) c_v^2 \lambda_{v-\varepsilon} \lambda_{\varepsilon} (\mathbf{C}_{\varepsilon, v-\varepsilon} \cdot \mathbf{k}) d\Omega d\mathbf{C}_{\varepsilon} d\mathbf{C}_{v-\varepsilon} d\varepsilon dv \\
&= \int_0^\infty \int_0^v \frac{1}{2} \psi_{\varepsilon, v-\varepsilon} n_{v-\varepsilon} n_{\varepsilon} g_{\varepsilon, v-\varepsilon} \frac{\sigma_{\varepsilon, v-\varepsilon}^2}{4} \iiint \frac{1}{2} (M_{v-\varepsilon} c_{v-\varepsilon}^2 + M_{\varepsilon} c_{\varepsilon}^2 + \frac{2m_{v-\varepsilon} m_{\varepsilon} c_{v-\varepsilon} c_{\varepsilon}}{m_{v-\varepsilon} + m_{\varepsilon}}) \lambda_{v-\varepsilon} \lambda_{\varepsilon} (\mathbf{C}_{\varepsilon, v-\varepsilon} \cdot \mathbf{k}) d\Omega d\mathbf{C}_{\varepsilon} d\mathbf{C}_{v-\varepsilon} d\varepsilon dv \\
&= \int_0^\infty \int_0^\infty \frac{1}{2} \psi_{\varepsilon, \zeta} n_{\zeta} n_{\varepsilon} g_{\varepsilon, \zeta} \frac{\sigma_{\varepsilon, \zeta}^2}{4} \iiint \frac{1}{2} (M_{\zeta} c_{\zeta}^2 + M_{\varepsilon} c_{\varepsilon}^2) \lambda_{\zeta} \lambda_{\varepsilon} (\mathbf{C}_{\varepsilon, \zeta} \cdot \mathbf{k}) d\Omega d\mathbf{C}_{\varepsilon} d\mathbf{C}_{\zeta} d\varepsilon d\zeta \\
&\quad + \int_0^\infty \int_0^\infty \frac{1}{2} \psi_{\varepsilon, \zeta} n_{\zeta} n_{\varepsilon} g_{\varepsilon, \zeta} \frac{\sigma_{\varepsilon, \zeta}^2}{4} \iiint \frac{1}{2} \frac{2m_{\zeta} m_{\varepsilon} c_{\zeta} c_{\varepsilon}}{m_{\zeta} + m_{\varepsilon}} \lambda_{\zeta} \lambda_{\varepsilon} (\mathbf{C}_{\varepsilon, \zeta} \cdot \mathbf{k}) d\Omega d\mathbf{C}_{\varepsilon} d\mathbf{C}_{\zeta} d\varepsilon d\zeta, \quad (36)
\end{aligned}$$

where  $v - \varepsilon = \zeta$ . As  $M_{\zeta} + M_{\varepsilon} = 1$ , in (36), this term

$$\int_0^\infty \int_0^\infty \frac{1}{2} \psi_{\varepsilon, \zeta} n_{\zeta} n_{\varepsilon} g_{\varepsilon, \zeta} \frac{\sigma_{\varepsilon, \zeta}^2}{4} \iiint \frac{1}{2} (M_{\zeta} c_{\zeta}^2 + M_{\varepsilon} c_{\varepsilon}^2) \lambda_{\zeta} \lambda_{\varepsilon} (\mathbf{C}_{\varepsilon, \zeta} \cdot \mathbf{k}) d\Omega d\mathbf{C}_{\varepsilon} d\mathbf{C}_{\zeta} d\varepsilon d\zeta$$

is cancelled with half of the integrated third term of the right hand side of (16) over  $v$  with  $\phi_v = m_v c_v^2/2$ , the kinetic energy dissipation due to aggregation,  $\Delta E_a$ , is then written as

$$\begin{aligned}
\Delta E_a &= \int_0^\infty \int_0^\infty \frac{1}{2} \psi_{\varepsilon, \zeta} n_{\zeta} n_{\varepsilon} g_{\varepsilon, \zeta} \frac{\sigma_{\varepsilon, \zeta}^2}{4} \iiint \frac{1}{2} \frac{2m_{\zeta} m_{\varepsilon} c_{\zeta} c_{\varepsilon}}{m_{\zeta} + m_{\varepsilon}} \\
&\quad \times \lambda_{\zeta} \lambda_{\varepsilon} (\mathbf{C}_{\varepsilon, \zeta} \cdot \mathbf{k}) d\Omega d\mathbf{C}_{\varepsilon} d\mathbf{C}_{\zeta} d\varepsilon d\zeta - \int_0^\infty \int_0^\infty \frac{1}{2} \psi_{\varepsilon, v} n_v n_{\varepsilon} g_{\varepsilon, v} \\
&\quad \times \frac{\sigma_{\varepsilon, v}^2}{4} \iiint \frac{1}{2} m_v c_v^2 \lambda_{v-\varepsilon} \lambda_{\varepsilon} (\mathbf{C}_{\varepsilon, v} \cdot \mathbf{k}) d\Omega d\mathbf{C}_{\varepsilon} d\mathbf{C}_v d\varepsilon dv. \quad (37)
\end{aligned}$$

It is worth pointing out in (37), as the integrations over all the size and velocity domains are being made,  $v$ ,  $\varepsilon$  and  $\zeta$  then become indistinguishable particles, thus,  $m_v c_v^2$  can be understood as  $\frac{m_{\zeta} c_{\zeta}^2}{m_{\zeta} + m_{\varepsilon}} + \frac{m_{\varepsilon} c_{\varepsilon}^2}{m_{\zeta} + m_{\varepsilon}}$ , then  $\Delta E_a \leq 0$ . With  $\mathbf{c}_{\zeta} = \mathbf{C}_{\zeta} + \mathbf{U}_s$ ,  $\mathbf{c}_{\varepsilon} = \mathbf{C}_{\varepsilon} + \mathbf{U}_s$ ,  $\mathbf{C}_{\zeta} = \mathbf{C}_c - M_{\varepsilon} \mathbf{c}_{\varepsilon} \zeta$  and  $\mathbf{C}_{\varepsilon} = \mathbf{C}_c + M_{\zeta} \mathbf{c}_{\varepsilon} \zeta$ , after the integrations over  $\Omega$  and  $\mathbf{C}$  carried out, (37) is

$$\Delta E_a = \int_0^\infty \int_0^\infty \psi_{\varepsilon, v} n_v n_{\varepsilon} g_{\varepsilon, v} \sigma_{\varepsilon, v}^2 \beta d\varepsilon dv, \quad (38)$$

where

$$\begin{aligned}
\beta &= \frac{1}{2(m_{\varepsilon} + m_v)} \sqrt{\frac{2\pi}{m_{\varepsilon} m_v}} \left\{ \left[ \frac{3\theta_s^3}{\sqrt{m_{\varepsilon} + m_v}} + \theta_s^{\frac{1}{2}} \sqrt{m_{\varepsilon} + m_v} u_s^2 \right. \right. \\
&\quad \left. \left. + \frac{4\sqrt{2}\theta_s(\mathbf{u}_s \cdot \mathbf{k})}{\sqrt{\pi}} \right] (m_{\varepsilon} - m_v) m_v + \frac{12\theta_s^{\frac{3}{2}} m_v^{\frac{3}{2}} m_{\varepsilon}}{\sqrt{m_{\varepsilon} + m_v}} \right. \\
&\quad \left. + \frac{8\theta_s^{\frac{3}{2}} m_{\varepsilon} (m_v - m_{\varepsilon})}{\sqrt{(m_{\varepsilon} + m_v)}} + \frac{3\sqrt{2}\pi}{2} \theta_s m_v^{\frac{3}{2}} m_{\varepsilon} (\mathbf{u}_s \cdot \mathbf{k}) \right\}. \quad (39)
\end{aligned}$$

The total kinetic energy dissipation due to inelastic collisions and aggregations, thus, becomes

$$\begin{aligned}
\Delta E_d &= \Delta E_c + \Delta E_a = \int_0^\infty \int_0^\infty n_v n_{\varepsilon} g_{\varepsilon, v} \sigma_{\varepsilon, v}^2 \\
&\quad \times [(1 - \psi_{\varepsilon, v})(e_{\varepsilon v}^2 - 1)\alpha + \psi_{\varepsilon, v} \beta] d\varepsilon dv, \quad (40)
\end{aligned}$$

where  $\alpha = \left[ \frac{8\pi\theta_s^3(m_{\varepsilon} + m_v)}{m_{\varepsilon} m_v} \right]^{\frac{1}{2}}$ . The mixture granular energy equation can then be expressed

$$\begin{aligned}
& \frac{3}{2} \left[ \frac{\partial(N\theta_s)}{\partial t} + \frac{\partial}{\partial \mathbf{r}} \cdot (N\theta_s \mathbf{u}_s) \right] + \frac{1}{2} \left[ \frac{\partial(\varepsilon_s \rho_s u_s^2)}{\partial t} + \frac{\partial}{\partial \mathbf{r}} \cdot (\varepsilon_s \rho_s u_s^2 \mathbf{u}_s) \right] \\
&+ \frac{\partial}{\partial \mathbf{r}} \cdot \mathbf{q}_s + P_s \frac{\partial}{\partial \mathbf{r}} \cdot \mathbf{u}_s + \bar{\tau}_s : \frac{\partial}{\partial \mathbf{r}} \mathbf{u}_s - \varepsilon_s \rho_s \langle (\mathbf{C}_v + \mathbf{u}_s) \cdot \mathbf{F}_v \rangle \\
&= \Delta E_d. \quad (41)
\end{aligned}$$

In this section, because the actual velocity  $\mathbf{c}_v$  is used and the completely inelastic collisions are taken into account in the derivation of the kinetic transport equations, the effects of the bulk velocity  $\mathbf{u}_s$  and the collision success factor on those transport properties particularly on those of the individual particle phases specified by their sizes are detailed. It can be seen in (21), (23a), (25), (33), and (41), by letting  $\psi_{\varepsilon v} = 0$ , those equation are then relaxed to the traditional ones in the classical kinetic theory of granular flow.<sup>24,25,27</sup>

### The Collision Frequency, Relative Velocity Distribution Function, and Collision Success Factor

It should be mentioned that the constitutive relations,<sup>7,24,27</sup> which are the properties of particles to do with the products of their velocities, for instance, the mathematical expressions for the normal pressure, stress tensor and heat flux, and the coefficients calculated in those products such as the shear and bulk viscosities and the granular heat conductivity, are not affected by the aggregation of particles thus remain the same in their forms and can be found in those references listed above. However, it must be pointed out that in granular flow systems where the aggregation of particles takes place, the values of those particle size related coefficients such as viscosities and conductivity are expected to change over time because the particle size is enlarged over time.

The collision frequency measures the number of collisions occurring to a particle in a unit time and a unit spatial volume. The number of collisions between particles  $v$ , and  $\varepsilon$ ,  $N_{\varepsilon v}$ , used to count the number of the collisions between the



two kinds of particles occurring in a unit time and spatial volume is expressed as

$$N_{ev} = n_v n_e g_{ev} \frac{\sigma_{ev}^2}{4} \iiint \lambda_v \lambda_e (\mathbf{C}_{ev} \cdot \mathbf{k}) d\Omega d\mathbf{C}_e d\mathbf{C}_v, \quad (42a)$$

after the integrations carried out, it then becomes

$$N_{ev} = N_v N_e g_{ev} \sigma_{ev}^2 \left[ \frac{8\pi\theta_s(m_v + m_e)}{m_v m_e} \right]^{\frac{1}{2}}, \quad (42b)$$

where  $N_v = n_v v$  and  $N_e = n_e e$  are the numbers of particles with size  $v$  and  $e$  per unit spatial volume, respectively. It should be noted that in (42a), for monodispersed systems, the right hand side of the expression should be multiplied by  $1/2$  to eliminate double counting. The collision frequencies of a particle  $v$  to all particles  $e$  and to all other particles can thus be given by (43a) and (43b), respectively.

$$F_{ev} = \frac{N_{ev}}{N_v} = N_e g_{ev} \sigma_{ev}^2 \left[ \frac{8\pi\theta_s(m_v + m_e)}{m_v m_e} \right]^{\frac{1}{2}}, \quad (43a)$$

$$F_v = \int_0^\infty n_e g_{ev} \sigma_{ev}^2 \left[ \frac{8\pi\theta_s(m_v + m_e)}{m_v m_e} \right]^{\frac{1}{2}} d\varepsilon. \quad (43b)$$

The collision success factor,  $\psi_{ev}$ , was introduced to quantify the fraction of the completely inelastic collisions between particles  $v$  and  $e$  such as that seen in (A3). It is used to calculate the number of the collisions between the two kinds of particles that leads to aggregation. From a more fundamental point of view, for a single collision between a particle  $v$  and a particle  $e$ ,  $\psi_{ev}$  gives the probability of this collision to succeed for an aggregation event.

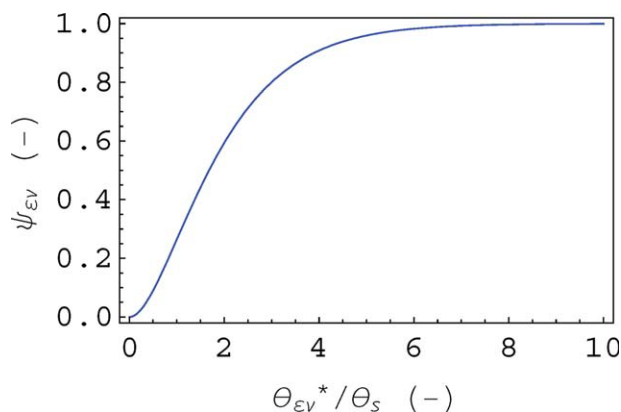
To obtain the analytical expression of  $\psi_{ev}$ , we now consider the collisions between particles  $v$  and  $e$ ,  $N_{ev}$ , as expressed in (42a); owing to  $d\mathbf{C}_v d\mathbf{C}_e = d\mathbf{C}_c d\mathbf{C}_{ev}$ , after the integration over the mass center velocity  $\mathbf{C}_c$  carried out, (42a) is then transformed into

$$N_{ev} = N_v N_e g_{ev} \sigma_{ev}^2 (2\pi)^2 \left[ \frac{m_e m_v}{2\pi(m_e + m_v)\theta_s} \right]^{\frac{3}{2}} \times \int_0^\infty C_{ev}^3 \exp \left[ -\frac{m_e m_v C_{ev}^2}{2(m_e + m_v)\theta_s} \right] dC_{ev}. \quad (44)$$

So,  $dN_{ev}/dC_{ev}$  is the relative velocity distribution function, which is a density function that interprets the collisions between particles  $v$  and  $e$  per unit spatial volume and time by the relative fluctuation velocity  $\mathbf{C}_{ev}$  between the two kinds of particles

$$\frac{dN_{ev}}{dC_{ev}} = N_v N_e g_{ev} \sigma_{ev}^2 (2\pi)^2 \left[ \frac{m_e m_v}{2\pi(m_e + m_v)\theta_s} \right]^{\frac{3}{2}} \times C_{ev}^3 \exp \left[ -\frac{m_e m_v C_{ev}^2}{2(m_e + m_v)\theta_s} \right]. \quad (45)$$

The normalized relative velocity distribution function  $f_{ev} = dN_{ev}/(N_{ev} dC_{ev})$  combined with (42b) is



**Figure 1.** Dependence of  $\psi_{ev}$  on  $\theta_{ev}^*/\theta_s$ .

[Color figure can be viewed in the online issue, which is available at [wileyonlinelibrary.com](http://wileyonlinelibrary.com).]

$$f_{ev} = \frac{N_v N_e g_{ev} \sigma_{ev}^2 (2\pi)^2 \left[ \frac{m_e m_v}{2\pi(m_e + m_v)\theta_s} \right]^{\frac{3}{2}} C_{ev}^3 \exp \left[ -\frac{m_e m_v C_{ev}^2}{2(m_e + m_v)\theta_s} \right]}{N_{ev}} = \frac{1}{2} \left[ \frac{m_e m_v}{(m_e + m_v)\theta_s} \right]^2 \exp \left[ -\frac{m_e m_v C_{ev}^2}{2(m_e + m_v)\theta_s} \right] C_{ev}^3. \quad (46)$$

According to Assumption 4, the collision success factor  $\psi_{ev}$  can thus be obtained by integrating the normalized relative velocity distribution function  $f_{ev}$  over the domain of  $C_{ev}$ ,  $[0, \mathbf{C}_{ev}^*]$ ; here  $\mathbf{C}_{ev}^*$  is the magnitude of the critical relative collision velocity  $\mathbf{C}_{ev}^*$ , then

$$\psi_{ev} = \int_0^{\mathbf{C}_{ev}^*} f_{ev} dC_{ev} = 1 - \left[ 1 + \frac{m_e m_v C_{ev}^{*2}}{2(m_e + m_v)\theta_s} \right] \times \exp \left[ -\frac{m_e m_v C_{ev}^{*2}}{2(m_e + m_v)\theta_s} \right]. \quad (47)$$

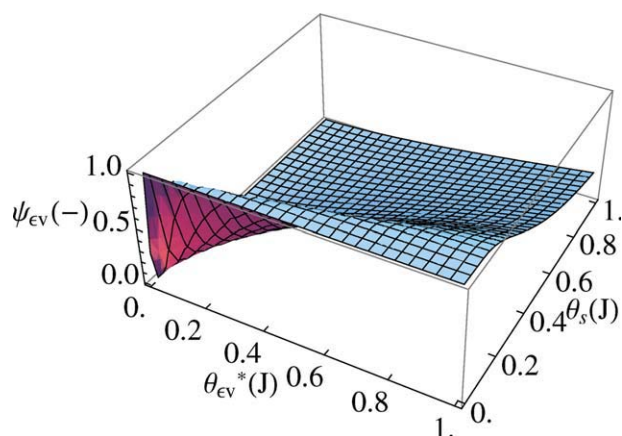
Equation 47 has clearly shown the dependence of the success factor on particle sizes (as the masses of particles  $v$  and  $e$ ,  $m_e$  and  $m_v$ , respectively, can be converted into their sizes) not only on the critical relative collision velocity and the mixture granular energy  $\theta_s$  of all particles in the system. Equation 47 also implies if  $\psi_{ev}$  and  $\theta_s$  are known, it can be used to calculate the critical relative collision velocity—an important attribute in characterizing the collisions of aggregating particles.

Defining a critical relative collision granular energy function,  $\theta_{ev}^* = \frac{m_e m_v C_{ev}^{*2}}{2(m_e + m_v)}$ , (47) becomes

$$\psi_{ev} = 1 - \left( 1 + \frac{\theta_{ev}^*}{\theta_s} \right) \exp \left( -\frac{\theta_{ev}^*}{\theta_s} \right). \quad (48)$$

As  $\theta_{ev}^*$  is the kinetic energy property of an individual collision and  $\theta_s$  is the mixture granular energy of all the particles in a granular flow system, (48) interprets that both the individual collision and the system's ensemble average kinetic energy characteristics determine the success of an aggregation. Figure 1 illustrates the change of  $\psi_{ev}$  in  $\theta_{ev}^*/\theta_s$ .

From Figure 1, it can be seen when the value of  $\theta_{ev}^*/\theta_s$  reaches around 3.0, the dramatic increase (to nearly 0.8) of  $\psi_{ev}$  starts changing to a rather slow pace, which indicates that efforts on increasing the value of  $\theta_{ev}^*/\theta_s$  to increase  $\psi_{ev}$  will then becomes almost inefficient and not worth



**Figure 2. Dependence of  $\psi_{ev}$  on  $\theta_{ev}^*$  and  $\theta_s$ .**

[Color figure can be viewed in the online issue, which is available at [wileyonlinelibrary.com](http://wileyonlinelibrary.com).]

experimenting. This figure can provide such useful information to identify the range of  $\psi_{ev}$  in which its large value can be achieved with little effort on increasing the ratio of  $\theta_{ev}^*/\theta_s$ .

When  $\theta_{ev}^*$  and  $\theta_s$  are regarded as the mutually independent variables, a 3D plot of  $\psi_{ev}$  vs.  $\theta_{ev}^*$  and  $\theta_s$  is given in Figure 2.

The significance of Figure 2 is that it is able to point out the direction quantitatively to which the best match of  $\theta_{ev}^*$  and  $\theta_s$  can give the most achievable  $\psi_{ev}$  value; for instance, in general as seen in this figure a large  $\theta_{ev}^*$  and a small  $\theta_s$  would give a large  $\psi_{ev}$ ; however, if large value of  $\theta_{ev}^*$  cannot be achieved, it is still possible to obtain a large value of  $\psi_{ev}$  with a small value of  $\theta_s$  even the chance is slim but can still occur (indicated in the down-left corner but on the upper surface of Figure 2).

If for a system, aggregation is to be avoided, Figures 1 and 2 can give useful information for how the least value of  $\psi_{ev}$  can be obtained by changing the values of  $\theta_{ev}^*$  and  $\theta_s$ .

It can also be suggested from Figures 1 and 2, because the collision success factor depends on the ratio of the critical relative collision granular energy to the mixture granular energy, under the condition that the flow of the granular particles can be maintained, the way to increase the efficiency of the successful aggregations is to increase the ratio by either reducing the turbulence of the granular flow system or increasing the critical velocity which for instance for a gas fluidized bed granulation system would be achieved by increasing the surface tension and viscosity of binders.<sup>44</sup> However, it may be worth pointing out that reducing system turbulence to increase the collision success factor should be taken cautiously as this may cause a system's momentum collapse (particles are not well suspended) thus particles may aggregate in a rather non-uniform way and their size distribution will not change in a gradually progressive fashion. The solution of the success factor suggests that increasing the critical relative velocity, or, using the particles and binding materials resulting in higher critical velocity, and keeping a degree of system turbulence to maintain the momentum of the particles can help increase the successful collisions efficiently.

It is also worth mentioning that (48) has established a link between the fundamental understanding of successful particle collisions leading to aggregation and the engineering processes of particle size enlargement owing to aggregation.

Equation 48 provides a method to quantitatively control the growth of particle size in granular flow systems.

As the normalized relative velocity distribution function  $f_{ev}$  is given by (46), it may be worth calculating the ensemble average relative velocity  $\langle C_{ev} \rangle$  that measures the intensity of a collision in an overall perspective.

$$\langle C_{ev} \rangle = \int_0^\infty C_{ev} f_{ev} dC_{ev} = \left[ \frac{72\pi(m_e + m_v)\theta_s}{m_e m_v} \right]^{\frac{1}{2}} \mathbf{k}. \quad (49)$$

It is seen in (49), the average collision intensity is related directly to the mixture granular energy of the granular flow system and the masses of the colliding particles.

## Concluding Remarks

The work presented in this article has given a mathematical description for the aggregation of particles in granular flow. It is seen from those derived kinetic transport equations that for a flow system where aggregation of the particles takes place, those conservative equations were shown to be able to describe the balances of the population, momentum, and kinetic energy of the particles characterized by their size and velocity. In particular, the number continuity equation is transformed into the typical population balance equation in the form of aggregation and growth; whereas the momentum and kinetic energy equations for the particles of the individual phases have shown the significance of the aggregation depending on the value of the collision success factor. It is expected that solving the three types of conservative equations together would give a complete prediction to the distributions of particle velocity, kinetic energy particularly to the size of particles for the systems where the motion of particles in spatial coordinates, that is, convection (segregation), and in their own sizes due to aggregation, are taking place simultaneously.

The dissipation of kinetic energy due to aggregations is expected to be highly related to the collision success factor, the mixture velocity, and granular energy of all particles. Moreover, for a single particle phase, it also depends on the sizes of the colliding particles.

The solution of collision success factor gives the probability of a collision to succeed for an aggregation from the kinetic energy point of view although the critical relative collision velocity needs further research to detail its dependency on processing materials and conditions. It is still true to say that the success factor can provide a quantitative way to practically control the coefficient of particle collisions that result in aggregation. It can thus be used to assess the efficiency of the process of particle aggregation in granular flow systems.

It needs to be mentioned that particle aggregation does not affect the mathematical forms of the constitutive relations; however, when the probability density function is extended to the higher orders of the Chapman-Enskog approximation, the corresponding terms associated with the integration of the velocity distribution function in the kinetic transport equations should also be re-evaluated particularly for the kinetic energy dissipation and the collision success factor.

Finally, it also needs to be pointed out that a validation of this theory is needed, which is presented in a subsequent

article on the application of the kinetic theory of aggregation to a gas fluidized bed granulation system.

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Financial support from the Unilever Vlaardingen Research Laboratory of the Netherlands and the University of Sheffield is gratefully acknowledged. Thanks also made to Professor M. J. Hounslow of the University of Sheffield for his valuable suggestions.

## Notation

### Roman symbols

$c$  = magnitude of actual velocity  $\mathbf{c}$  ( $\text{m s}^{-1}$ )  
 $C$  = magnitude of fluctuation velocity  $\mathbf{C}$  ( $\text{m s}^{-1}$ )  
 $e$  = restitution coefficient in the collision between particles (–)  
 $f$  = velocity–size distribution function ( $\text{s}^3 \text{m}^{-9}$ )  
 $F$  = collision frequency ( $\text{s}^{-1}$ )  
 $g$  = radial distribution function (–)  
 $m$  = mass of a particle (kg)  
 $M$  = mass ratio of a particle to the total mass of the pair of colliding particles (–)  
 $n$  = number density of particles ( $\text{m}^{-6}$ )  
 $N$  = total number of particles per unit volume ( $\text{m}^{-3}$ )  
 $N_{\varepsilon v}$  = total number of collisions between particles  $\varepsilon$  and  $v$  per unit time and volume ( $\text{m}^{-3} \text{s}^{-1}$ )  
 $P$  = normal pressure of particles ( $\text{Pa m}^{-3}$ )  
 $r$  = collision rate of particles ( $\text{s}^4 \text{m}^{-10}$ )  
 $t$  = time (s)  
 $v$  = the size of individual particles in volume ( $\text{m}^3$ )

### Vectors

$\mathbf{c}$  = actual velocity of particles ( $\text{m s}^{-1}$ )  
 $\mathbf{C}$  = fluctuation velocity of particles ( $\text{m s}^{-1}$ )  
 $\mathbf{F}$  = the external force (N)  
 $\mathbf{G}$  = growth rate of particles in volume size ( $\text{m}^3 \text{s}^{-1}$ )  
 $\mathbf{k}$  = unit vector (–)  
 $\mathbf{q}$  = heat flux ( $\text{W m}^{-5}$ )  
 $\mathbf{r}$  = spatial position vector (m)  
 $\mathbf{u}$  = ensemble average velocity ( $\text{m s}^{-1}$ )  
 $\mathbf{w}$  = number density weighted diffusion velocity of particles ( $\text{m s}^{-1}$ )

### Tensors

$\bar{\mathbf{I}}$  = unit tensor (–)  
 $\bar{\boldsymbol{\tau}}$  = stress tensor ( $\text{Pa m}^{-3}$ )

### Greek letters

$\Delta$  = change of properties  
 $\varepsilon$  = the size of individual particles in volume ( $\text{m}^3$ )  
 $\phi$  = property of particles in terms of their velocity  
 $\varphi$  = the filling angle in spherical coordinates (rad)  
 $\lambda$  = normalized velocity–size distribution function of particles ( $\text{s m}^{-4}$ )  
 $\Omega$  = solid angle (rad)  
 $\psi$  = collision success factor (–)  
 $\rho$  = density of particles ( $\text{kg m}^{-3}$ )  
 $\sigma$  = interdistance of two colliding particles (m)  
 $\theta$  = granular energy of particles (J)  
 $\omega$  = the filling angles in spherical coordinates (rad)  
 $\chi$  = Taylor's expansion  
 $\xi$  = property of particles by volume size  
 $\zeta$  = dummy variable for  $v - \varepsilon$  ( $\text{m}^3$ )

### Superscripts

' = reverse collision  
 \* = critical property

### Subscripts

$s$  = ensemble particles  
 $v$  = the size of individual particles in volume  
 $\varepsilon$  = the size of individual particles in volume  
 $\varepsilon v$  = collisions between particles  $\varepsilon$  and  $v$

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## Appendix

The detailed derivation of the collision rate is presented in the work of Liu,<sup>44</sup> in the following only a concise version of such a derivation is given.

Consider two kinds of particles with sizes  $v$  and  $\varepsilon$ , respectively, having collisions based on the mechanism of binary collision<sup>1</sup> (Assumption 2) in differential elements  $d\Omega d\mathbf{c}_v d\mathbf{v} d\mathbf{c}_\varepsilon d\boldsymbol{\varepsilon} d\mathbf{r} dt$ , the rate of the forward collisions, which results in the decrease of the number of particles characterized by  $\mathbf{c}_v$ , is expressed in (A1). This expression also takes into the sizes of the colliding particles, i.e., if a particle  $v$  is situated at position  $\mathbf{r}$  then the colliding particle  $\varepsilon$  must be at  $\mathbf{r} + \sigma_{ev}\mathbf{k}$ .

$$f_v f_\varepsilon (\mathbf{r} + \sigma_{ev}\mathbf{k}) g_{ev} \frac{\sigma_{ev}^2}{4} (\mathbf{c}_{ev} \cdot \mathbf{k}) d\Omega d\mathbf{c}_v d\mathbf{v} d\mathbf{c}_\varepsilon d\boldsymbol{\varepsilon} d\mathbf{r} dt, \quad (\text{A1})$$

Using Taylor's expansion for  $f_\varepsilon(\mathbf{r} + \sigma_{ev}\mathbf{k})$ , (A1) becomes

$$f_v f_\varepsilon \chi_{ev} g_{ev} \frac{\sigma_{ev}^2}{4} (\mathbf{c}_{ev} \cdot \mathbf{k}) d\Omega d\mathbf{c}_v d\mathbf{v} d\mathbf{c}_\varepsilon d\boldsymbol{\varepsilon} d\mathbf{r} dt, \quad (\text{A2})$$

$$\text{where } \chi_{ev} = \left[ 1 + \sum_m \frac{1}{m!} \left( \sigma_{ev}\mathbf{k} \cdot \frac{\partial}{\partial \mathbf{r}} \right)^m f_\varepsilon \right].$$

According to Assumption 1 that some fraction  $\psi_{ev}$  of the collisions occurred in a completely inelastic way that leads to aggregation, (A2) can then be transformed into

$$(1 - \psi_{ev}) f_v f_\varepsilon \chi_{ev} g_{ev} \frac{\sigma_{ev}^2}{4} (\mathbf{c}_{ev} \cdot \mathbf{k}) d\Omega d\mathbf{c}_v d\mathbf{v} d\mathbf{c}_\varepsilon d\boldsymbol{\varepsilon} d\mathbf{r} dt + \psi_{ev} f_v f_\varepsilon \chi_{ev} g_{ev} \frac{\sigma_{ev}^2}{4} (\mathbf{c}_{ev} \cdot \mathbf{k}) d\Omega d\mathbf{c}_v d\mathbf{v} d\mathbf{c}_\varepsilon d\boldsymbol{\varepsilon} d\mathbf{r} dt. \quad (\text{A3})$$

Similarly, the collisions between particles  $v$  and  $\varepsilon$  with reverse velocities  $\mathbf{c}'_\varepsilon$  and  $\mathbf{c}'_v$ , respectively, resulting in the increase of the number of particles  $v$  characterized by  $\mathbf{c}_v$ , taking into account the completely inelastic collisions, can be expressed

$$(1 - \psi'_{ev}) f'_v f'_\varepsilon \chi'_{ev} g'_{ev} \frac{\sigma_{ev}^2}{4} (\mathbf{c}'_{ev} \cdot \mathbf{k}') d\Omega' d\mathbf{c}'_v d\mathbf{v} d\mathbf{c}'_\varepsilon d\boldsymbol{\varepsilon}' d\mathbf{r}' dt, \quad (\text{A4})$$

where the symbols with “'” refer to the properties of the reverse collisions.

We also have the following relations

$$d\Omega' = d\Omega, \sigma'_{ev} = \sigma_{ev}, \mathbf{c}'_{ev} = -e_{ev}\mathbf{c}_{ev}, \mathbf{k}' = -\mathbf{k},$$

$$\mathbf{c}'_\varepsilon = \mathbf{c}_v + M_\varepsilon(1 + e_{ev})\mathbf{c}_{ev}, \mathbf{c}'_v = \mathbf{c}_\varepsilon - M_v(1 + e_{ev})\mathbf{c}_{ev}, \quad (\text{A5})$$

$$d\mathbf{c}'_\varepsilon d\mathbf{c}'_v = \left| \frac{\partial(\mathbf{c}'_\varepsilon, \mathbf{c}'_v)}{\partial(\mathbf{c}_v, \mathbf{c}_\varepsilon)} \right| d\mathbf{c}_v d\mathbf{c}_\varepsilon = e_{ev}.$$



Subtracting (A3) from (A4) yields the net increase of the number of particles  $v$  characterized by  $\mathbf{c}_v$ . Also according to the relations in (A5), we have

$$\begin{aligned} & [e_{ev}^2 (1 - \psi'_{ev}) f'_v f'_\varepsilon \chi'_{ev} g'_{ev} - (1 - \psi_{ev}) f_v f_\varepsilon \chi_{ev} g_{ev}] \\ & \times \frac{\sigma_{ev}^2}{4} (\mathbf{c}_{ev} \cdot \mathbf{k}) d\Omega d\mathbf{c}_v dv d\mathbf{c}_\varepsilon d\varepsilon d\mathbf{r} dt - \psi_{ev} f_v f_\varepsilon \chi_{ev} g_{ev} \\ & \frac{\sigma_{ev}^2}{4} (\mathbf{c}_{ev} \cdot \mathbf{k}) d\Omega d\mathbf{c}_v dv d\mathbf{c}_\varepsilon d\varepsilon d\mathbf{r} dt. \quad (\text{A6}) \end{aligned}$$

It is clear that the completely inelastic collisions between particles  $v - \varepsilon$  and  $\varepsilon$  can also result in the net increase of the number of particles  $v$ . This is given by

$$\frac{1}{2} \psi_{e,v-\varepsilon} f_{v-\varepsilon} f_\varepsilon \chi_{e,v-\varepsilon} g_{e,v-\varepsilon} \frac{\sigma_{e,v-\varepsilon}^2}{4} (\mathbf{c}_{e,v-\varepsilon} \cdot \mathbf{k}) d\Omega d\mathbf{c}_{v-\varepsilon} dv d\mathbf{c}_\varepsilon d\varepsilon d\mathbf{r} dt, \quad (\text{A7})$$

where  $1/2$  eliminates the double counting of the collisions, and,  $\varepsilon$  ranges from 0 to  $v$ . It is worth pointing out that there is no reverse collisions between particles  $v - \varepsilon$  and  $\varepsilon$  contributing to the increase of the number of particles  $v$  as (A7) is only concerned with the size characteristic of  $f_{v-\varepsilon}$  and  $f_\varepsilon$ . (A7) can also be transformed into

$$\frac{1}{2M_{v-\varepsilon}^2} \psi_{e,v-\varepsilon} f_{v-\varepsilon} f_\varepsilon \chi_{e,v-\varepsilon} g_{e,v-\varepsilon} \frac{\sigma_{e,v-\varepsilon}^2}{4} (\mathbf{c}_{e,v-\varepsilon} \cdot \mathbf{k}) d\Omega d\mathbf{c}_{v-\varepsilon} dv d\mathbf{c}_\varepsilon d\varepsilon d\mathbf{r} dt. \quad (\text{A8})$$

This is because

$$\begin{aligned} \mathbf{c}_v &= M_\varepsilon \mathbf{c}_\varepsilon + M_{v-\varepsilon} \mathbf{c}_{v-\varepsilon}, \mathbf{c}_{v-\varepsilon} = \mathbf{c}_v - M_\varepsilon \mathbf{c}_{e,v-\varepsilon}, \mathbf{c}_\varepsilon \\ &= \mathbf{c}_v + M_{v-\varepsilon} \mathbf{c}_{e,v-\varepsilon}, \mathbf{c}_{e,v-\varepsilon} = \frac{\mathbf{c}_{ev}}{M_{v-\varepsilon}}, d(v - \varepsilon) \\ &= dv, d\mathbf{c}_{v-\varepsilon} d\mathbf{c}_\varepsilon = \left| \frac{\partial(\mathbf{c}_{v-\varepsilon}, \mathbf{c}_\varepsilon)}{\partial(\mathbf{c}_v, \mathbf{c}_\varepsilon)} \right| d\mathbf{c}_v d\mathbf{c}_\varepsilon = \frac{1}{M_{v-\varepsilon}} d\mathbf{c}_v d\mathbf{c}_\varepsilon, \quad (\text{A9}) \end{aligned}$$

where  $\mathbf{c}_v$  is the mass center velocity of particles  $v - \varepsilon$  and  $\varepsilon$ , that is, the velocity of particles  $v$ .

Adding (A8) into (A6) yields the differential form of the number of collisions occurring to particles  $v$  to give the net increase of the number of particles  $v$  in terms of their size  $v$  and velocity  $\mathbf{c}_v$  characteristics. With the integrations over the domains of  $\Omega$ ,  $\mathbf{c}_\varepsilon$  and  $\varepsilon$ , the total number of collisions occurring to particles  $v$  per unit time and spatial volume is obtained.

$$\begin{aligned} r_v &= \iiint [e_{ev}^2 (1 - \psi'_{ev}) f'_v f'_\varepsilon \chi'_{ev} g'_{ev} - (1 - \psi_{ev}) f_v f_\varepsilon \chi_{ev} g_{ev}] \\ &\times \frac{\sigma_{ev}^2}{4} (\mathbf{c}_{ev} \cdot \mathbf{k}) d\Omega d\mathbf{c}_\varepsilon d\varepsilon + \int_0^v \iint \frac{1}{2M_{v-\varepsilon}^2} \psi_{e,v-\varepsilon} f_{v-\varepsilon} f_\varepsilon \chi_{e,v-\varepsilon} g_{e,v-\varepsilon} \\ &\frac{\sigma_{e,v-\varepsilon}^2}{4} (\mathbf{c}_{e,v-\varepsilon} \cdot \mathbf{k}) d\Omega d\mathbf{c}_\varepsilon d\varepsilon - \iiint \psi_{ev} f_v f_\varepsilon \chi_{ev} g_{ev} \frac{\sigma_{ev}^2}{4} (\mathbf{c}_{ev} \cdot \mathbf{k}) d\Omega d\mathbf{c}_\varepsilon d\varepsilon. \quad (\text{A10}) \end{aligned}$$

As can be seen from (A10), the first term of the right hand side is the net birth rate contributing to the velocity characteristic of  $f_v$ ; the second and third terms together give the net birth rate of particles contributing to the size characteristic of  $f_v$ .

For a property  $\phi_v$  of particles  $v$  in terms of their velocity  $\mathbf{c}_v$ , the change of the property due to the collisions occurring to particles  $v$  is expressed as  $\int \phi_v r_v d\mathbf{c}_v$ ; therefore, according to (A10), the transport Eq. 11a is obtained

$$\begin{aligned} & \frac{\partial(n_v \langle \phi_v \rangle)}{\partial t} + \frac{\partial}{\partial \mathbf{r}} \cdot n_v \langle \phi_v \mathbf{c}_v \rangle - n_v \left\langle \frac{\partial \phi_v}{\partial t} \right\rangle - n_v \left\langle \frac{\partial \phi_v}{\partial \mathbf{r}} \cdot \mathbf{c}_v \right\rangle \\ & - n_v \left\langle \frac{\partial \phi_v}{\partial \mathbf{c}_v} \cdot \frac{\mathbf{F}_v}{m_v} \right\rangle + \frac{\partial}{\partial v \mathbf{k}} \cdot n_v \langle \phi_v \mathbf{G}_v \rangle - \left\langle \frac{\partial \phi_v}{\partial v \mathbf{k}} \right\rangle \cdot n_v \mathbf{G}_v \\ & = \iiint (\phi'_v - \phi_v) (1 - \psi_{ev}) f_v f_\varepsilon \chi_{ev} g_{ev} \frac{\sigma_{ev}^2}{4} (\mathbf{c}_{ev} \cdot \mathbf{k}) d\varepsilon d\Omega d\mathbf{c}_\varepsilon d\mathbf{c}_v \\ & + \iiint \phi_v \left[ \int_0^v \frac{1}{2M_{v-\varepsilon}^2} \psi_{e,v-\varepsilon} f_{v-\varepsilon} f_\varepsilon \chi_{e,v-\varepsilon} g_{e,v-\varepsilon} \frac{\sigma_{e,v-\varepsilon}^2}{4} (\mathbf{c}_{e,v-\varepsilon} \cdot \mathbf{k}) d\varepsilon \right. \\ & \left. - \int_0^\infty \psi_{e,v} f_v f_\varepsilon \chi_{ev} g_{ev} \frac{\sigma_{ev}^2}{4} (\mathbf{c}_{ev} \cdot \mathbf{k}) d\varepsilon \right] d\Omega d\mathbf{c}_\varepsilon d\mathbf{c}_v, \quad (\text{A11}) \end{aligned}$$

where the first term on the right hand side of (A11) is gained due to

$$\begin{aligned} & \iiint \phi_v e_{ev}^2 (1 - \psi'_{ev}) f'_v f'_\varepsilon \chi'_{ev} g'_{ev} \frac{\sigma_{ev}^2}{4} (\mathbf{c}_{ev} \cdot \mathbf{k}) d\Omega d\mathbf{c}_\varepsilon d\varepsilon d\mathbf{c}_v \\ & = \iiint \phi_v (1 - \psi'_{ev}) f'_v f'_\varepsilon \chi'_{ev} g'_{ev} \frac{\sigma_{ev}^2}{4} (\mathbf{c}'_{ev} \cdot \mathbf{k}') d\Omega' d\mathbf{c}'_\varepsilon d\varepsilon d\mathbf{c}'_v \\ & = \iiint \phi'_v (1 - \psi_{ev}) f_v f_\varepsilon \chi_{ev} g_{ev} \frac{\sigma_{ev}^2}{4} (\mathbf{c}_{ev} \cdot \mathbf{k}) d\Omega d\mathbf{c}_\varepsilon d\varepsilon d\mathbf{c}_v, \quad (\text{A12}) \end{aligned}$$

where  $\phi'_v$  is the property of particles  $v$  after collisions and is the function of variables  $(\Omega', \mathbf{c}'_\varepsilon, \mathbf{c}'_v)$ . (A12) can be understood that  $\phi_v$  is being transported by the reverse collisions occurring to particles  $v$ . Since every reverse collision must corresponds to a forward collision, the properties with variable groups  $(\Omega', \mathbf{c}'_\varepsilon, \mathbf{c}'_v)$  and  $(\Omega, \mathbf{c}_\varepsilon, \mathbf{c}_v)$  can be exchanged<sup>7</sup> also  $g_{ev} = g'_{ev}$  as the radial distribution function is considered to relate to the volume fraction of all particles only.<sup>7,9,10,58</sup>

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